# TRAFFIC IMPACT STUDY 

For<br>PN Restaurants<br>Proposed Popeye's Restaurant with Drive-Thru

Property Located at:
197 South Plank Road (NYS Route 52)
Parcel 60-3-6.1
Town of Newburgh, Orange County, NY

Prepared by:
DYNAMIC TRAFFIC

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## INTRODUCTION

It is proposed to construct a Popeye's restaurant with drive-thru on a parcel of land currently developed with a Dairy Queen, located on the southwest corner of the intersection of Union Avenue (NYS Route 300) and South Plank Road (NYS Route 52) in the Town of Newburgh, Orange County, New York (see Figure 1 in Appendix A). The site is designated as Parcel 60-3-6.1 on the Town of Newburgh Tax Maps. The existing use consists of a building with a 2,342 SF Dairy Queen. It is proposed to raze the existing site and construct a 2,537 SF Popeye's Restaurant ("The Project"). The site is located within the Zone B - Business Zone. Access to the site is currently provided via an enter only driveway along South Plank Road (NYS Route 52) and a full movement driveway along Union Avenue (NYS Route 300). It is proposed to close the existing access points and provide access to the site via a new full movement driveway along Union Avenue (NYS Route 300) and a right-turn in/right-turn driveway along South Plank Road (NYS Route 52).

Dynamic Traffic LLC has been retained to prepare this study to assess the traffic impact associated with the construction of The Project on the adjacent roadway network. This study documents the methodology, analyses, findings and conclusions of our study and includes:

- A detailed field inspection was conducted to obtain an inventory of existing roadway geometry, traffic control, and location and geometry of existing driveways and intersections.
- Existing traffic data was collected via manual turning movement (MTM) counts during the weekday PM, and Saturday midday peak periods at the intersection of South Plank Road (NYS Route 52) and Union Avenue (NYS Route 300).
- Projections of traffic to be generated by the proposed development were prepared utilizing trip generation data as published by the Institute of Transportation Engineers. Site traffic was then assigned to the adjacent street system based upon the anticipated directional distribution.
- Capacity analyses were conducted for the Existing, No Build, and Build conditions for the study intersections.
- The proposed points of ingress and egress were inspected for adequacy of geometric design, spacing and/or alignment to streets and driveways on the opposite side of the street, relationship to other driveways adjacent to the development, and conformance with accepted design standards.
- The site plan as designed was reviewed for sufficiency in accommodating large wheel base vehicles such as delivery trucks, refuse trucks, and emergency vehicles.
- The parking layout and supply was assessed based on accepted design standards, local requirements, and demand experienced at similar developments.


## EXISTING CONDITIONS

A review of the existing roadway conditions near the proposed site was conducted to provide the basis for assessing the traffic impact of the development. This included field investigations of the surrounding roadways and intersections, collection of traffic volume data, and extensive analyses.

## Existing Roadway Conditions

The following are descriptions of the roadways in the study area:
Union Avenue (NYS Route 300) is an Urban Minor Arterial roadway under NYSDOT jurisdiction with a general north/south orientation. In the vicinity of the site the posted speed limit is 40 MPH and the roadway provides one travel lane in each direction with a two-way center left-turn lane south of the intersection with South Plank Road (NYS Route 52). On-street parking is not permitted. Curb and sidewalk are provided in the vicinity of the intersection with South Plank Road (NYS Route 52). Union Avenue (NYS Route 300) provides a straight horizontal alignment along the site frontage and a general downgrade from north to south. The land uses along Union Avenue (NYS Route 300) in the vicinity of The Project are primarily commercial.

South Plank Road (NYS Route 52) is an Urban Minor Arterial roadway under NYSDOT jurisdiction with a general east/west orientation. In the vicinity of the site the posted speed limit is 40 MPH and the roadway provides one travel lane in each direction. On-street parking is not permitted. Curb and sidewalk are provided in the vicinity of the intersection with Union Avenue (NYS Route 300). South Plank Road (NYS Route 52) provides a straight horizontal alignment along the site frontage and a relatively flat vertical alignment. The land uses along South Plank Road (NYS Route 52) in the vicinity of The Project are primarily commercial.

## Existing Traffic Volumes

Manual turning movement (MTM) counts were conducted on Thursday, October 20, 2022 from 4:30 to 6:30 PM as well as on Saturday, October 22, 2022 from 11:00 AM to 2:00 PM at the intersection of South Plank Road (NYS Route 52) and Union Avenue (NYS Route 300).

Review of the collected traffic data reveals that the weekday evening PSH occurs between 4:45-5:45 PM and the Saturday PSH occurs between 12:30 PM - 1:30 PM. Figure 2, located in Appendix A, shows the existing peak hour traffic volumes at the study intersections. All traffic counts are contained in Appendix B.

## Existing Capacity Analysis

The methodology utilized in the capacity analyses is described in the Highway Capacity Manual, published by the Transportation Research Board. In general, the term Level of Service (LOS) is used to provide a "qualitative" evaluation of capacity based upon certain "quantitative" calculations related to empirical values, such as traffic volume and intersection control.

At signalized intersections, factors that affect the various approach capacities include width of approach, number of lanes, signal "green time", turning percentages, truck volumes, etc. However, delays cannot be related to capacity in a simple one-to-one fashion. For example, it is possible to have delays in the Level of Service "F" range without exceeding roadway capacity. Substantial delays can exist without exceeding capacity if one or more of the following conditions exist: long signal cycle lengths; a particular traffic movement experiences a long red time; or progressive movement for a particular lane group is poor. Table I describes the level of service ranges for signalized intersections.

An unsignalized (STOP sign controlled) driveway or side street along a through route is seldom critical from an overall capacity standpoint, however, it may be of great significance to the capacity of the minor cross-route, and it may influence the quality of traffic flow on both. When analyzing an unsignalized intersection, it is assumed that both the major street through and right turn movements are unimpeded and have the right-of-way over all side street traffic and left turns from the major street. All other turning movements in the intersection cross, merge with, or are otherwise impeded by major street movements. Traffic delays at unsignalized intersections are determined by sequentially processing these impeded movements. Table II describes the level of service ranges for unsignalized (stop controlled) intersections.

Table I
Level of Service Criteria
for Signalized Intersections

| Level of <br> Service | Average Control Delay <br> (seconds per vehicle) |
| :---: | :---: |
| A | 0.0 to 10.0 |
| B | 10.1 to 20.0 |
| C | 20.1 to 35.0 |
| D | 35.1 to 55.0 |
| E | 55.1 to 80.0 |
| F | greater than 80.0 |

Table II
Level of Service Criteria
for Unsignalized Intersections

| Level of <br> Service | Average Control Delay <br> (seconds per vehicle) |
| :---: | :---: |
| a | 0.0 to 10.0 |
| b | 10.1 to 15.0 |
| c | 15.1 to 25.0 |
| d | 25.1 to 35.0 |
| e | 35.1 to 50.0 |
| f | greater than 50.0 |

It should be noted that the analyses within the Highway Capacity Manual assume a random arrival for all the movements, which may not be the case if an adjacent traffic signal is present that platoons vehicles, such as the signalized intersection of Union Avenue (NYS Route 300) \& South Plank Road (NYS Route 52).

All capacity analyses were performed utilizing Synchro 11 software. It should be noted that the existing percentage of trucks and peak hour factors were used in the existing analysis. Table III summarizes the existing levels of service (LOS) and delays. All capacity analysis calculation worksheets are contained in Appendix C.

Table III
Existing Levels of Service

| Intersection | Direction/ <br> Movement |  | PM PSH |  | SAT PSH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS | V/C | LOS | V/C |
| South Plank Road (NYS Route 52) \& Union Avenue (NYS Route 300) | EB | LTR | E (62.5) | 0.96 | D (39.6) | 0.79 |
|  | WB | LT | C (31.7) | 0.63 | C (29.8) | 0.43 |
|  | WB | R | A (9.3) | 0.14 | A (6.6) | 0.14 |
|  | NB | L | C (30.5) | 0.77 | C (33.9) | 0.76 |
|  | N | TR | C (32.3) | 0.77 | C (27.2) | 0.68 |
|  | SB | L | B (15.2) | 0.34 | B (12.6) | 0.25 |
|  | SB | TR | D (36.1) | 0.79 | D (40.7) | 0.86 |
|  |  | rall | D (37.6) | 0.97 | C (33.0) | 0.86 |

A (\#) - Signalized Intersection Level of Service (seconds of delay per vehicle)
The following are discussions pertaining to each of the existing intersections analyzed.

## Union Avenue (NYS Route 300) \& South Plank Road (NYS Route 52)

South Plank Road (NYS Route 52) intersects Union Avenue (NYS Route 300) to form a four-leg intersection controlled by a traffic signal. The signal timing directive was obtained from NYS DOT which indicates that a three-phase cycle is utilized with a 115 -second cycle length during both peak hours. The eastbound approach of South Plank Road (NYS Route 52) provides a shared left turn/through/right turn lane while the westbound approach provides a shared left turn/through lane and a dedicated right turn lane. The northbound and southbound approaches of Union Avenue (NYS Route 300) both provide a dedicated left turn lane and a shared through/right turn lane. The traffic signal permit plan and timing directive are contained in Appendix B.

A review of the existing analysis reveals that the intersection operates at levels of service " $D$ " or better and all movements operate at levels of service "E" or better during the analyzed peak periods. See Table III for the individual movement levels of service and delays.

## FUTURE CONDITIONS

Traffic volumes and operational analyses were developed for both the 2026 No Build and 2026 Build conditions. The No Build conditions provide a baseline for assessing the impact of the site development traffic on the roadway system. The process of developing the No Build and Build traffic volumes and the subsequent analyses is outlined below.

Regardless of whether the subject site is developed or not, traffic volumes on the surrounding roadways are expected to increase as a result of developments throughout the region. A growth rate of $2.0 \%$ per year was applied to the study area intersections.

Through consultation with the Town of Newburgh Planning Board staff, there are eleven other developments in the vicinity of the site that have been approved but not yet constructed that are identified as potential significant traffic generators.

- A residential development consisting of 246 units known as the Polo Club, located at 1582 Union Avenue (NYS Route 300), has been approved and is currently under construction. Projections of the associated traffic volumes were developed utilizing data from Traffic Impact Study, prepared by Maser Consulting and dated December 9, 2019. It should be noted that this study only includes traffic projections for the weekday morning and evening peak hours. As such, traffic projections for the Saturday midday peak hour were developed utilizing the Institute of Transportation Engineers' (ITE) Land Use Code (LUC) 220 - Multi-Family Housing. The Adjacent Development Traffic Volumes are shown on Figure 3.
- A development consisting of a 290,000 SF warehouse, located along South Plank Road (NYS Route 52) just north of Jeanne Drive, has been approved but not yet constructed. Projections of the associated traffic volumes were developed utilizing data from Traffic Study, prepared by JMC Project 18156 and dated December 3, 2020. It should be noted that this study only includes traffic projections for the weekday morning and evening peak hours. As such, traffic projections for the Saturday midday peak hour were developed utilizing the Institute of Transportation Engineers' (ITE) Land Use Code (LUC) 150 - Warehousing. The Adjacent Development Traffic Volumes are shown on Figure 4.
- A development consisting of a 100 -unit senior adult housing facility and a $3,150 \mathrm{SF}$ bank known as Monarch Woods, located at 25 Monarch Drive, has been approved but not yet constructed. Projections of the associated traffic volumes were developed by utilizing the Institute of Transportation Engineers' (ITE) Land Use Code (LUC) 252 - Senior Adult Housing and LUC 912 - Drive-In Bank. The Adjacent Development Traffic Volumes are shown on Figure 5.
- A development consisting of two warehouse buildings totaling 1,142,200 SF known as Matrix Logistics Center, located opposite the Newburgh Mall, has been approved and is currently under construction. Projections of the associated traffic volumes were developed utilizing data published within the Traffic Impact Study, prepared by Langan Engineering and dated May 14, 2021. It should be noted that this study only includes traffic projections for the weekday morning and evening peak hours. As such, traffic projections for the Saturday midday peak hour were developed utilizing the Institute of Transportation Engineers' (ITE) Land Use Code (LUC) 150 - Warehousing. The Adjacent Development Traffic Volumes are shown on Figure 6.
- A residential development consisting of 246 apartments known as The Enclave, located at 1565 Union Avenue (NYS Route 300), has been approved and not yet constructed. Projections of the associated traffic volumes were developed using ITE LUC 220 - Multifamily Housing. The Adjacent Development Traffic Volumes are shown on Figure 7.
- A development known as Resorts World Casino, located within the Newburgh Mall, has been approved and opened. Projections of the associated traffic volumes were developed utilizing data published within a memo by Maser Consulting dated February 12, 2021. Traffic projections for the weekday PM peak hour and Saturday peak hour were developed utilizing the traffic generation as shown in the aforementioned memo through ITE LUC 473 Casino/Video Lottery Establishment. The Adjacent Development Traffic Volumes are shown on Figure 8.
- A development consisting of a 20,000 SF office and retail known as MJKC, located off of NYS Route 32 has been approved but not yet constructed. Projections of the associated traffic volumes were developed using ITE LUC 822 - Strip Retail Plaza ( $<40 \mathrm{~K}$ ). The Adjacent Traffic Volumes are shown on Figure 9.
- A development consisting of a 173,000 SF warehouse known as MKJ Park Warehouse, located off of NYS Route 32, has been approved but not yet constructed. Projections of the associated traffic volumes were developed using data published within the Traffic Impact Study, prepared by Colliers Engineering \& Design, dated April 6, 2023. It should be noted that this study only includes traffic projections for the weekday morning and evening peak hours. As such, traffic projections for the Saturday midday peak hour were developed using ITE LUC 150 - Warehouse. The Adjacent Development Traffic Volumes are shown in Figure 10.
- A development consisting of a $56,000 \mathrm{SF}$ warehouse known as Fabulous Events, located along NYS Route 32, has been approved but not yet constructed. Projections of the associated traffic volumes were developed using data published within the Traffic Impact Study, prepared by Colliers Engineering \& Design, dated May 26, 2023. It should be noted that this study only includes traffic projections for the weekday morning and evening peak hours. As such, traffic projections for the Saturday midday peak hour were developed using ITE LUC 150 Warehouse. The Adjacent Development Traffic Volumes are shown in Figure 11.
- A development consisting of a 3,515 SF clinic known as WellNow, located at 1425 Route 300, has been constructed but not yet filled. Projections of the associated traffic volumes were developed using ITE LUC 720 - Medical-Dental Office Building - Stand Alone. The Adjacent Traffic Volumes are shown on Figure 12.
- A development consisting of an 85,000 SF self-storage known as SAM Newburgh, located at 1420 Route 300, is still under review. Projections of the associated traffic volumes were developed using ITE LUC 151 - Mini-Warehouse. The Adjacent Traffic Volumes are shown on Figure 13.

Future No Build traffic volumes were developed by applying the background growth rate of $2.0 \%$ for two (2) years to the study area roadways existing traffic volumes. Figure 14, in Appendix A, shows the No Build traffic volumes.

## Traffic Generation

Trip generation projections for The Project were prepared utilizing trip generation research data as published under Land Use Code 934 - Fast-Food Restaurant with Drive-Through Window in the Institute of Transportation Engineers' (ITE) publication, Trip Generation, $11^{\text {th }}$ Edition. This publication sets forth trip generation rates based on empirical traffic count data conducted at numerous research sites.

According to studies conducted by ITE, traffic associated with LUC 934 is not $100 \%$ newly generated. Rather, a portion of the traffic is diverted from the existing traffic stream on the adjacent roadway network. This is because the Popeye's is not exclusively a destination land use, instead patrons stop on their way to/from other locations such as home or work. ITE identifies a $55 \%$ passby traffic percentage, and was used during the evening peak hour. It should be noted that there will be passby traffic during the Saturday midday peak period and this passby rate was set at $50 \%$, consistent with the weekday morning peak hour. Table IV below details the traffic volumes associated with the subject project taking into account internal capture and the passby credits.

Table IV
Trip Generation Considering Passby Traffic

| Land Use | Trip Type | PM PSH |  |  | SAT PSH |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | In | Out | Total | In | Out | Total |
| 2,537 SF Fast-Food Restaurant <br> with Drive-Through Window | Total | 44 | 40 | 84 | 71 | 69 | 140 |
|  | Passby | 24 | 22 | 46 | 36 | 34 | 70 |
|  | New (Primary) | $\mathbf{2 0}$ | $\mathbf{1 8}$ | $\mathbf{3 8}$ | $\mathbf{3 5}$ | $\mathbf{3 5}$ | $\mathbf{7 0}$ |

Once the magnitude of traffic to be generated by the site is known, it is necessary to assign that traffic to the adjacent street system. The distribution of new traffic to the surrounding roadways is based on the location of primary arterial roadways, major signalized intersections and existing traffic patterns. Figures 15-19, located in Appendix A, illustrate the Primary Traffic Trip Distribution, Primary Site Generated Volumes, Passby Traffic Trip Distribution, Passby Site Generated Volumes, and the Total Site Generated Volumes, respectively. The Total Site Generated Volumes assigned to the study area network were added to the No Build traffic volumes to generate the Build traffic volumes, which are shown in Figure 20.

## Trip Generation Comparison

As previously noted, the site is currently occupied by a Dairy Queen which has an existing trip generation. As counts were not conducted at the existing Dairy Queen driveways, trip generation research data as published under Land Use Code 934 - Fast-Food Restaurant with Drive-Through Window in the Institute of Transportation Engineers' (ITE) publication, Trip Generation, $11^{\text {th }}$ Edition was utilized. Table $V$ below provides a comparison between the trips associated with the existing site and the trips projected for the proposed redevelopment.

Table V
Existing vs. Proposed Trip Generation Comparison

| Land Use | PM PSH |  |  | SAT PSH |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | In | Out | Total | In | Out | Total |
| Fast-Food Restaurant with Drive-Through <br> Window - Dairy Queen (Existing) | 40 | 37 | 77 | 66 | 63 | 129 |
| Fast-Food Restaurant with Drive-Through <br> Window - Popeye's (Proposed) | 44 | 40 | 84 | 71 | 69 | 140 |
| Difference | $\mathbf{+ 4}$ | $\mathbf{+ 3}$ | $\mathbf{+ 7}$ | $\mathbf{+ 5}$ | $\mathbf{+ 6}$ | $\mathbf{+ 1 1}$ |

As shown in the table above, it is anticipated that 7 additional trips during the weekday evening peak hour and 11 additional trips during the Saturday midday peak hour are anticipated to access the site from the adjacent roadway network with the proposed redevelopment.

## Future Capacity Analysis

Operational conditions at the study intersections were analyzed under the No Build and Build conditions and are summarized in Table VI below.

Table VI
Future Levels of Service

| Intersection | Direction/ <br> Movement |  | PM PSH |  |  |  |  |  | SAT PSH |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | No Build |  | Build |  | Build w/ Mit. |  | No Build |  | Build |  | Build w/ Mit. |  |
|  |  |  | LOS | V/C | LOS | V/C | LOS | V/C | LOS | V/C | LOS | V/C | LOS | V/C |
| South Plank <br> Road (NYS <br> Route 52) \& Union <br> Avenue <br> (NYS Route 300) | EB | LTR | F (412.4) | 1.83 | F (443.5) | 1.90 | F (419.4) | 1.85 | F (156.2) | 1.23 | F (177.3) | 1.28 | F (158.6) | 1.24 |
|  | WB | LT | D (54.5) | 0.86 | E (65.6) | 0.93 | E (62.5) | 0.91 | D (40.6) | 0.61 | D (46.3) | 0.70 | $\mathrm{D}(43.9)$ | 0.67 |
|  | WB | R | B (11.6) | 0.21 | B (11.8) | 0.21 | B (11.4) | 0.21 | A (6.2) | 0.20 | A (6.2) | 0.20 | A (5.9) | 0.20 |
|  | NB | L | F (96.7) | 1.06 | F (110.1) | 1.10 | F (110.6) | 1.10 | F (137.5) | 1.15 | F (165.5) | 1.23 | F (147.3) | 1.18 |
|  | NB | TR | D (43.2) | 0.91 | D (43.4) | 0.91 | D (45.4) | 0.92 | C (32.5) | . 080 | C (32.6) | 0.80 | C (34.7) | 0.81 |
|  | SB | L | C (23.1) | 0.52 | C (23.4) | 0.52 | C (23.3) | 0.52 | B (18.2) | 0.47 | B (18.2) | 0.47 | C (20.8) | 0.49 |
|  | SB | TR | D (39.6) | 0.86 | D (39.8) | 0.87 | D (43.5) | 0.89 | D (47.5) | 0.93 | D (47.9) | 0.93 | D (53.9) | 0.95 |
|  | Overall |  | F (118.8) | 1.84 | F (127.9) | 1.90 | F (124.2) | 1.85 | E (70.1) | 1.24 | E (78.1) | 1.29 | E (74.6) | 1.24 |
| Union <br> Avenue | EB | LR | - | - | c (25.1) | 0.163 | - | - | - | - | d (28.8) | 0.287 | - | - |
| (NYS Route | NB | LT | - | - | a (10.0) | 0.025 | - | - | - | - | b (10.5) | 0.045 | - | - |
| 300) \& Site Driveway | Overall |  | - | - | a (0.5) | - | - | - | - | - | a (1.0) | - | - | - |
| South Plank Road (NYS | NB | R | - | - | b (12.5) | 0.017 | - | - | - | - | b (11.9) | 0.023 | - | - |
| Route 52) \& Site Driveway | Overall |  | - | - | a (0.1) | - | - | - | - | - | a (0.1) | - | - | - |

a (\#) - Unsignalized Intersection Level of Service (seconds of delay per vehicle)
A (\#) - Signalized Intersection Level of Service (seconds of delay per vehicle)

## South Plank Road (NYS Route 52) \& Union Avenue (NYS Route 300)

With the addition of site generated traffic, the intersection is anticipated to operate at overall intersection No Build levels of service " $F$ " during the analyzed peak hours. Additionally, each movement is anticipated to operate at No Build levels of service.

Revised signal timings were investigated based on the new traffic volumes for both peak hours. Specifically, the reallocation of one (1) second from the northbound/southbound ROW (phase 1 and 5) to the northbound/southbound lead lefts (phase 2 and 6), in addition to one (1) second from the northbound/southbound ROW (phase 1 and 5) to the eastbound/westbound ROW (phase 3) is recommended during the weekday evening peak hour. Additionally, the reallocation of one (1) second from the northbound/southbound ROW (phase 1 and 5) to the northbound /southbound lead lefts (phase 2 and 6), in addition to two (2) seconds from the northbound/southbound ROW (phase 1 and 5) to the eastbound/westbound ROW (phase 3) is recommended during the Saturday peak hour. It should be noted that with these signal timing modifications, the intersection anticipated to operate at similar or better than No Build levels of service. See Table VI for the individual movement levels of service and delays.

## Union Avenue (NYS Route 300) \& Site Driveway

The site driveway is proposed to intersect Union Avenue (NYS Route 300) to form an unsignalized T-intersection with the eastbound approach of the site driveway operating under stop control. The eastbound approach of the site driveway is proposed to provide a shared left turn/right turn lane. The northbound approach of Union Avenue (NYS Route 300) is proposed to provide a dedicated left turn lane via the existing two-way center left-turn lane and a dedicated through lane. The southbound approach of Union Avenue (NYS Route 300) is proposed to provide a shared through/right turn lane. As designed, the driveway is anticipated to operate at levels of service " D " or better during the studied peak hours. See Table VI for the individual movement levels of service and delays.

## South Plank Road (NYS Route 52) \& Site Driveway

The site driveway is proposed to intersect South Plank Road (NYS Route 52) to form an unsignalized T -intersection with the northbound approach of the site driveway operating under stop control. The eastbound approach of South Plank Road (NYS Route 52) is proposed to provide a shared through/right turn lane. The westbound approach of South Plank Road (NYS Route 52) is proposed to provide a dedicated through lane. The northbound approach of the site driveway is proposed to provide a dedicated right turn lane.

As designed, the driveway is anticipated to operate at levels of service " $B$ " during the studied peak hours. See Table VI for the individual movement levels of service and delays.

## SITE PLAN

## Site Access and Circulation

The site plan was reviewed with respect to the site access and on-site circulation design. As noted previously, access to The Project will be provided via a new full movement driveway along Union Avenue (NYS Route 300) and a new full movement driveway along South Plank Road (NYS Route 52).

The parking lot will be serviced by parking aisles with widths of 18 ', which will allow for one way circulation and 60 degree parking.

The drive-thru lanes will operate in a counter clockwise direction with the ability to stack fourteen (14) cars in the drive-thru lane. Drive-thru counts conducted by this firm for three Popeye's locations in New Jersey found an average maximum queue length of eight (8) vehicles within the drive-thru and a maximum queue length of ten (10) vehicles. Therefore, the proposed drive-thru design will provide adequate stacking for the maximum anticipated demand. A bypass lane is also be provided to ensure adequate and efficient circulation and to ensure that drive-thru queues do not impact on site circulation for patrons who park and walk in to the restaurant.

## Parking

The Town of Newburgh Ordinance sets forth a parking requirement of 1 parking space per 4 seats for restaurants and fast food establishments. The Ordinance also states a requirement of 1 space per 40 SF. This equates to a parking requirement of 6 spaces for the proposed 24 -seat Popeye's restaurant. The site as proposed provides 22 spaces and as such, the Ordinance requirement is met.

An Operational Characteristics Study has been conducted by Dynamic Traffic for Popeye's sites which identified a maximum parking demand of 6.48 spaces per $1,000 \mathrm{SF}$, and equates to a parking demand of 16 spaces for the proposed 2,537 SF Popeye's (inclusive of employees). Consequently, the proposed 22 parking spaces will be sufficient to support the anticipated demand of the project.

It is proposed to provide parking stalls with dimensions of $9^{\prime} \times 18^{\prime}$, which satisfy the Ordinance minimum requirement of $9^{\prime} \times 18^{\prime}$.

## FINDINGS \& CONCLUSIONS

## Findings

Based upon the detailed analyses as documented herein, the following findings are noted:

- The proposed 2,537 SF Popeye's Restaurant is projected to generate 20 entering trips and 18 exiting trips during the evening peak hour, and 35 entering trips and 35 exiting trips during the Saturday peak hour that are "new" to the adjacent roadway network.
- Access to the site is proposed to be provided via a right-turn in/right-turn out driveway along South Plank Road (NYS Route 52) and a new full movement driveway along Union Avenue (NYS Route 300).
- With the addition of site generated traffic and proposed signal retiming, the intersection of Union Avenue (NYS Route 300) and South Plank Road (NYS Route 52) is anticipated to operate at overall No Build intersection level of service " $F$ " during the peak hours studied.
- As designed, the intersection of Union Avenue (NYS Route 300) and the site driveway is anticipated to operate at levels of service "D" or better during the peak hours studied.
- As designed, the intersection of South Plank Road (NYS Route 52) and the site driveway is anticipated to operate at levels of service " $B$ " during the peak hours studied.
- As proposed, The Project's site driveways and internal circulation have been designed to provide for safe and efficient movement of automobiles and large wheel base vehicles.
- The proposed parking supply and design is sufficient to support the projected demand and satisfies the Ordinance requirements.


## Conclusions

Based upon our Traffic Impact Study as detailed in the body of this report, it is the professional opinion of Dynamic Traffic LLC that the adjacent street system of the Town of Newburgh and NYSDOT will not experience any significant degradation in operating conditions with the construction of The Project. The site driveways are located to provide safe and efficient access to the adjacent roadway system. The site plan as proposed provides for good circulation throughout the site and provides adequate parking to accommodate The Project's needs.

Appendix A
Traffic Volume Figures




Proposed Popeye's Development
Traffic Impact Study
1021-22-01537

Figure 3
Adjacent Development Traffic Volumes [The Polo Club - 1582 Route 300]



Proposed Popeye's Development
Traffic Impact Study
1021-22-01537



Proposed Popeye's Development
Traffic Impact Study
1021-22-01537
Figure 7
Adjacent Development Traffic Volumes
[The Enclave - 1565 Route 300]





Proposed Popeye's Development
Traffic Impact Study
1021-22-01537










## Appendix B Project Information

# Dynamic Traffic, LLC <br> 1904 Main Street, Lake Como, NJ 07719 <br> 245 Main Street - Suite \#110, Chester, NJ 07930 <br> 732-681-0760 

E/W: South Plank Rd
N/S: Union Ave
Town/County: Newburgh/Orange
Job \#: 1021-22-01537

File Name: South Plank Rd \& Union Ave - PM
Site Code : 00000000
Start Date : 10/20/2022
Page No : 1

| Groups Printed- Cars - Trucks (SU) - Trucks (TT) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | T Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | South Plank Road Eastbound |  |  |  |  | South Plank Road Westbound |  |  |  |  | Union Avenue Northbound |  |  |  |  | Union Avenue Southbound |  |  |  |  |  |
| Start Time | Left | Thru | Right | Peds | App. Total | Left | Thru | Right | Peds | App. Total | Left | Thru | Right | Peds | App. Total | Left | Thru | Right | Peds | App. Total |  |
| 04:30 PM | 22 | 59 | 30 | 0 | 111 | 12 | 86 | 23 | 0 | 121 | 60 | 122 | 8 | 0 | 190 | 19 | 111 | 30 | 0 | 160 | 582 |
| 04:45 PM | 17 | 50 | 40 | 0 | 107 | 11 | 91 | 30 | 0 | 132 | 61 | 137 | 11 | 0 | 209 | 22 | 120 | 23 | 0 | 165 | 613 |
| Total | 39 | 109 | 70 | 0 | 218 | 23 | 177 | 53 | 0 | 253 | 121 | 259 | 19 | 0 | 399 | 41 | 231 | 53 | 0 | 325 | 1195 |
| 05:00 PM | 17 | 78 | 39 | 0 | 134 | 16 | 100 | 27 | 1 | 144 | 49 | 132 | 15 | 0 | 196 | 16 | 97 | 14 | 0 | 127 | 601 |
| 05:15 PM | 11 | 68 | 47 | 0 | 126 | 9 | 71 | 14 | 0 | 94 | 65 | 172 | 6 | 0 | 243 | 19 | 109 | 14 | 0 | 142 | 605 |
| 05:30 PM | 24 | 63 | 40 | 0 | 127 | 8 | 79 | 19 | 0 | 106 | 79 | 140 | 13 | 0 | 232 | 22 | 92 | 20 | 0 | 134 | 599 |
| 05:45 PM | 15 | 54 | 37 | 0 | 106 | 5 | 72 | 21 | 0 | 98 | 52 | 123 | 22 | 0 | 197 | 22 | 117 | 24 | 0 | 163 | 564 |
| Total | 67 | 263 | 163 | 0 | 493 | 38 | 322 | 81 | 1 | 442 | 245 | 567 | 56 | 0 | 868 | 79 | 415 | 72 | 0 | 566 | 2369 |
| 06:00 PM | 9 | 57 | 31 | 0 | 97 | 8 | 63 | 12 | 0 | 83 | 66 | 133 | 12 | 0 | 211 | 14 | 110 | 14 | 0 | 138 | 529 |
| 06:15 PM | 15 | 44 | 28 | 0 | 87 | 7 | 70 | 18 | 0 | 95 | 59 | 119 | 14 | 0 | 192 | 20 | 97 | 18 | 0 | 135 | 509 |
| Grand Total | 130 | 473 | 292 | 0 | 895 | 76 | 632 | 164 | 1 | 873 | 491 | 1078 | 101 | 0 | 1670 | 154 | 853 | 157 | 0 | 1164 | 4602 |
| Apprch \% | 14.5 | 52.8 | 32.6 | 0 |  | 8.7 | 72.4 | 18.8 | 0.1 |  | 29.4 | 64.6 | 6 | 0 |  | 13.2 | 73.3 | 13.5 | 0 |  |  |
| Total \% | 2.8 | 10.3 | 6.3 | 0 | 19.4 | 1.7 | 13.7 | 3.6 | 0 | 19 | 10.7 | 23.4 | 2.2 | 0 | 36.3 | 3.3 | 18.5 | 3.4 | 0 | 25.3 |  |
| Cars | 129 | 462 | 286 | 0 | 877 | 74 | 626 | 161 | 1 | 862 | 483 | 1065 | 100 | 0 | 1648 | 150 | 842 | 152 | 0 | 1144 | 4531 |
| \% Cars | 99.2 | 97.7 | 97.9 | 0 | 98 | 97.4 | 99.1 | 98.2 | 100 | 98.7 | 98.4 | 98.8 | 99 | 0 | 98.7 | 97.4 | 98.7 | 96.8 | 0 | 98.3 | 98.5 |
| Trucks (SU) | 1 | 11 | 3 | 0 | 15 | 2 | 5 | 2 | 0 | 9 | 3 | 11 | 1 | 0 | 15 | 2 | 9 | 4 | 0 | 15 | 54 |
| \% Trucks (SU) | 0.8 | 2.3 | 1 | 0 | 1.7 | 2.6 | 0.8 | 1.2 | 0 | 1 | 0.6 | 1 | 1 | 0 | 0.9 | 1.3 | 1.1 | 2.5 | 0 | 1.3 | 1.2 |
| Trucks (TT) | 0 | 0 | 3 | 0 | 3 | 0 | 1 | 1 | 0 | 2 | 5 | 2 | 0 | 0 | 7 | 2 | 2 | 1 | 0 | 5 | 17 |
| \% Trucks (TT) | 0 | 0 | 1 | 0 | 0.3 | 0 | 0.2 | 0.6 | 0 | 0.2 | 1 | 0.2 | 0 | 0 | 0.4 | 1.3 | 0.2 | 0.6 | 0 | 0.4 | 0.4 |


|  | South Plank Road Eastbound |  |  |  |  | South Plank Road Westbound |  |  |  |  | Union Avenue Northbound |  |  |  |  | Union Avenue Southbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start <br> Time | Left | Thru | Right | Peds | App. Total | Left | Thru | Right | Peds | App. Total | Left | Thru | Right | Peds | App. Total | Left | Thru | Right | Peds | App. Total | Int. Total |
| Peak Hour Analysis From 04:30 PM to 06:15 PM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 04:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 04:45 PM | 17 | 50 | 40 | 0 | 107 | 11 | 91 | 30 | 0 | 132 | 61 | 137 | 11 | 0 | 209 | 22 | 120 | 23 | 0 | 165 | 613 |
| 05:00 PM | 17 | 78 | 39 | 0 | 134 | 16 | 100 | 27 | 1 | 144 | 49 | 132 | 15 | 0 | 196 | 16 | 97 | 14 | 0 | 127 | 601 |
| 05:15 PM | 11 | 68 | 47 | 0 | 126 | 9 | 71 | 14 | 0 | 94 | 65 | 172 | 6 | 0 | 243 | 19 | 109 | 14 | 0 | 142 | 605 |
| 05:30 PM | 24 | 63 | 40 | 0 | 127 | 8 | 79 | 19 | 0 | 106 | 79 | 140 | 13 | 0 | 232 | 22 | 92 | 20 | 0 | 134 | 599 |
| Total Volume | 69 | 259 | 166 | 0 | 494 | 44 | 341 | 90 | 1 | 476 | 254 | 581 | 45 | 0 | 880 | 79 | 418 | 71 | 0 | 568 | 2418 |
| \% App. Total | 14 | 52.4 | 33.6 | 0 |  | 9.2 | 71.6 | 18.9 | 0.2 |  | 28.9 | 66 | 5.1 | 0 |  | 13.9 | 73.6 | 12.5 | 0 |  |  |
| PHF | . 719 | . 830 | . 883 | . 000 | . 922 | . 688 | . 853 | . 750 | . 250 | . 826 | . 804 | . 844 | . 750 | . 000 | . 905 | . 898 | . 871 | . 772 | 000 | . 861 | . 986 |
| Cars | 68 | 250 | 165 | 0 | 483 | 43 | 337 | 89 | 1 | 470 | 251 | 573 | 44 | 0 | 868 | 77 | 411 | 70 | 0 | 558 | 2379 |
| \% Cars | 98.6 | 96.5 | 99.4 | 0 | 97.8 | 97.7 | 98.8 | 98.9 | 100 | 98.7 | 98.8 | 98.6 | 97.8 | 0 | 98.6 | 97.5 | 98.3 | 98.6 | 0 | 98.2 | 98.4 |
| Trucks (SU) | 1 | 9 | 0 | 0 | 10 | 1 | 3 | 0 | 0 | 4 | 1 | 6 | 1 | 0 | 8 | 2 | 6 | 1 | 0 | 9 | 31 |
| \% Trucks (SU) | 1.4 | 3.5 | 0 | 0 | 2.0 | 2.3 | 0.9 | 0 | 0 | 0.8 | 0.4 | 1.0 | 2.2 | 0 | 0.9 | 2.5 | 1.4 | 1.4 | 0 | 1.6 | 1.3 |
| Trucks (TT) | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 1 | 0 | 2 | 2 | 2 | 0 | 0 | 4 | 0 | 1 | 0 | 0 | 1 | 8 |
| \% Trucks (TT) | 0 | 0 | 0.6 | 0 | 0.2 | 0 | 0.3 | 1.1 | 0 | 0.4 | 0.8 | 0.3 | 0 | 0 | 0.5 | 0 | 0.2 | 0 | 0 | 0.2 | 0.3 |

# Dynamic Traffic, LLC <br> 1904 Main Street, Lake Como, NJ 07719 <br> 245 Main Street - Suite \#110, Chester, NJ 07930 <br> 732-681-0760 

E/W: South Plank Rd
N/S: Union Ave
Town/County: Newburgh/Orange
Job \#: 1021-22-01537

File Name : South Plank Rd \& Union Ave - SAT
Site Code : 00000000
Start Date: 10/22/2022
Page No : 1

Groups Printed- Cars - Trucks (SU) - Trucks (TT)

|  | South Plank Road Eastbound |  |  |  |  | South Plank Road Westbound |  |  |  |  | Union Avenue Northbound |  |  |  |  | Union Avenue Southbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | Peds | App. Total | Left | Thru | Right | Peds | App. Total | Left | Thru | Right | Peds | App. Total | Left | Thru | Right | Peds | App. Total | Int. Total |
| 11:00 AM | 16 | 54 | 51 | 1 | 122 | 8 | 47 | 20 | 0 | 75 | 53 | 109 | 19 | 0 | 181 | 14 | 114 | 21 | 0 | 149 | 527 |
| 11:15 AM | 25 | 52 | 44 | 0 | 121 | 11 | 33 | 16 | 0 | 60 | 53 | 130 | 12 | 0 | 195 | 22 | 113 | 25 | 0 | 160 | 536 |
| 11:30 AM | 16 | 59 | 57 | 0 | 132 | 12 | 62 | 26 | 0 | 100 | 43 | 127 | 12 | 0 | 182 | 22 | 126 | 14 | 0 | 162 | 576 |
| 11:45 AM | 15 | 40 | 48 | 0 | 103 | 6 | 36 | 16 | 0 | 58 | 32 | 145 | 17 | 0 | 194 | 24 | 132 | 22 | 0 | 178 | 533 |
| Total | 72 | 205 | 200 | 1 | 478 | 37 | 178 | 78 | 0 | 293 | 181 | 511 | 60 | 0 | 752 | 82 | 485 | 82 | 0 | 649 | 2172 |
| 12:00 PM | 13 | 41 | 61 | 0 | 115 | 12 | 59 | 21 | 0 | 92 | 60 | 117 | 15 | 0 | 192 | 16 | 115 | 11 | 0 | 142 | 541 |
| 12:15 PM | 14 | 43 | 37 | 0 | 94 | 8 | 41 | 21 | 0 | 70 | 56 | 140 | 21 | 0 | 217 | 17 | 125 | 16 | 0 | 158 | 539 |
| 12:30 PM | 19 | 35 | 49 | 0 | 103 | 13 | 38 | 21 | 0 | 72 | 57 | 139 | 11 | 0 | 207 | 21 | 142 | 19 | 0 | 182 | 564 |
| 12:45 PM | 20 | 54 | 49 | 0 | 123 | 14 | 46 | 26 | 0 | 86 | 56 | 129 | 7 | 0 | 192 | 19 | 119 | 4 | 0 | 142 | 543 |
| Total | 66 | 173 | 196 | 0 | 435 | 47 | 184 | 89 | 0 | 320 | 229 | 525 | 54 | 0 | 808 | 73 | 501 | 50 | 0 | 624 | 2187 |
| 01:00 PM | 22 | 64 | 35 | 0 | 121 | 8 | 43 | 18 | 0 | 69 | 44 | 136 | 11 | 0 | 191 | 16 | 124 | 22 | 0 | 162 | 543 |
| 01:15 PM | 12 | 48 | 53 | 0 | 113 | 12 | 46 | 21 | 0 | 79 | 56 | 149 | 8 | 0 | 213 | 15 | 137 | 16 | 0 | 168 | 573 |
| 01:30 PM | 18 | 44 | 43 | 2 | 107 | 7 | 46 | 20 | 0 | 73 | 52 | 153 | 17 | 0 | 222 | 20 | 99 | 13 | 0 | 132 | 534 |
| 01:45 PM | 18 | 48 | 37 | 0 | 103 | 8 | 54 | 10 | 0 | 72 | 40 | 119 | 12 | 0 | 171 | 17 | 111 | 13 | 0 | 141 | 487 |
| Total | 70 | 204 | 168 | 2 | 444 | 35 | 189 | 69 | 0 | 293 | 192 | 557 | 48 | 0 | 797 | 68 | 471 | 64 | 0 | 603 | 2137 |
| Grand Total | 208 | 582 | 564 | 3 | 1357 | 119 | 551 | 236 | 0 | 906 | 602 | 1593 | 162 | 0 | 2357 | 223 | 1457 | 196 | 0 | 1876 | 6496 |
| Apprch \% | 15.3 | 42.9 | 41.6 | 0.2 |  | 13.1 | 60.8 | 26 | 0 |  | 25.5 | 67.6 | 6.9 | 0 |  | 11.9 | 77.7 | 10.4 | 0 |  |  |
| Total \% | 3.2 | 9 | 8.7 | 0 | 20.9 | 1.8 | 8.5 | 3.6 | 0 | 13.9 | 9.3 | 24.5 | 2.5 | 0 | 36.3 | 3.4 | 22.4 | 3 | 0 | 28.9 |  |
| Cars | 206 | 579 | 560 | 3 | 1348 | 118 | 548 | 235 | 0 | 901 | 598 | 1587 | 161 | 0 | 2346 | 223 | 1446 | 192 | 0 | 1861 | 6456 |
| \% Cars | 99 | 99.5 | 99.3 | 100 | 99.3 | 99.2 | 99.5 | 99.6 | 0 | 99.4 | 99.3 | 99.6 | 99.4 | 0 | 99.5 | 100 | 99.2 | 98 | 0 | 99.2 | 99.4 |
| Trucks (SU) | 1 | 2 | 3 | 0 | 6 | 1 | 1 | 1 | 0 | 3 | 4 | 4 | 1 | 0 | 9 | 0 | 9 | 3 | 0 | 12 | 30 |
| \% Trucks (SU) | 0.5 | 0.3 | 0.5 | 0 | 0.4 | 0.8 | 0.2 | 0.4 | 0 | 0.3 | 0.7 | 0.3 | 0.6 | 0 | 0.4 | 0 | 0.6 | 1.5 | 0 | 0.6 | 0.5 |
| Trucks (TT) | 1 | 1 | 1 | 0 | 3 | 0 | 2 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 2 | 0 | 2 | 1 | 0 | 3 | 10 |
| \% Trucks (TT) | 0.5 | 0.2 | 0.2 | 0 | 0.2 | 0 | 0.4 | 0 | 0 | 0.2 | 0 | 0.1 | 0 | 0 | 0.1 | 0 | 0.1 | 0.5 | 0 | 0.2 | 0.2 |

# Dynamic Traffic, LLC <br> 1904 Main Street, Lake Como, NJ 07719 <br> 245 Main Street - Suite \#110, Chester, NJ 07930 <br> 732-681-0760 

E/W: South Plank Rd
N/S: Union Ave
Town/County: Newburgh/Orange
Job \#: 1021-22-01537
File Name : South Plank Rd \& Union Ave - SAT
Site Code : 00000000
Start Date : 10/22/2022
Page No : 2

|  | South Plank Road Eastbound |  |  |  |  | South Plank Road Westbound |  |  |  |  | Union Avenue Northbound |  |  |  |  | Union Avenue Southbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | Peds | App. Total | Left | Thru | Right | Peds | App. Total | Left | Thru | Right | Peds | App. Total | Left | Thru | Right | Peds | App. Total | Int. Total |
| Peak Hour Analysis From 11:00 AM to 01:45 PM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 12:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 12:30 PM | 19 | 35 | 49 | 0 | 103 | 13 | 38 | 21 | 0 | 72 | 57 | 139 | 11 | 0 | 207 | 21 | 142 | 19 | 0 | 182 | 564 |
| 12:45 PM | 20 | 54 | 49 | 0 | 123 | 14 | 46 | 26 | 0 | 86 | 56 | 129 | 7 | 0 | 192 | 19 | 119 | 4 | 0 | 142 | 543 |
| 01:00 PM | 22 | 64 | 35 | 0 | 121 | 8 | 43 | 18 | 0 | 69 | 44 | 136 | 11 | 0 | 191 | 16 | 124 | 22 | 0 | 162 | 543 |
| 01:15 PM | 12 | 48 | 53 | 0 | 113 | 12 | 46 | 21 | 0 | 79 | 56 | 149 | 8 | 0 | 213 | 15 | 137 | 16 | 0 | 168 | 573 |
| Total Volume | 73 | 201 | 186 | 0 | 460 | 47 | 173 | 86 | 0 | 306 | 213 | 553 | 37 | 0 | 803 | 71 | 522 | 61 | 0 | 654 | 2223 |
| \% App. Total | 15.9 | 43.7 | 40.4 | 0 |  | 15.4 | 56.5 | 28.1 | 0 |  | 26.5 | 68.9 | 4.6 | 0 |  | 10.9 | 79.8 | 9.3 | 0 |  |  |
| PHF | . 830 | . 785 | . 877 | . 000 | . 935 | . 839 | . 940 | . 827 | . 000 | . 890 | . 934 | . 928 | . 841 | . 000 | . 942 | . 845 | . 919 | . 693 | . 000 | . 898 | . 970 |
| Cars | 73 | 200 | 183 | 0 | 456 | 47 | 171 | 86 | 0 | 304 | 211 | 550 | 37 | 0 | 798 | 71 | 519 | 59 | 0 | 649 | 2207 |
| \% Cars | 100 | 99.5 | 98.4 | 0 | 99.1 | 100 | 98.8 | 100 | 0 | 99.3 | 99.1 | 99.5 | 100 | 0 | 99.4 | 100 | 99.4 | 96.7 | 0 | 99.2 | 99.3 |
| Trucks (SU) | 0 | 1 | 2 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 4 | 0 | 3 | 1 | 0 | 4 | 11 |
| \% Trucks (SU) | 0 | 0.5 | 1.1 | 0 | 0.7 | 0 | 0 | 0 | 0 | 0 | 0.9 | 0.4 | 0 | 0 | 0.5 | 0 | 0.6 | 1.6 | 0 | 0.6 | 0.5 |
| Trucks (TT) | 0 | 0 | 1 | 0 | 1 | 0 | 2 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 5 |
| \% Trucks (TT) | 0 | 0 | 0.5 | 0 | 0.2 | 0 | 1.2 | 0 | 0 | 0.7 | 0 | 0.2 | 0 | 0 | 0.1 | 0 | 0 | 1.6 | 0 | 0.2 | 0.2 |



Peak Hour Factor Calculation

| Source Intersection Traffic Volumes |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interval | EB |  |  | WB |  |  | NB |  |  | SB |  |  | Total |
|  | L | T | R | L | T | R | L | T | R | L | T | R |  |
| 0-15 min. |  |  | 40 | 11 |  |  | 61 | 137 | 11 |  | 120 |  | 380 |
| $15-30 \mathrm{~min}$. |  |  | 39 | 16 |  |  | 49 | 132 | 15 |  | 97 |  | 348 |
| 30-45 min. |  |  | 47 | 9 |  |  | 65 | 172 | 6 |  | 109 |  | 408 |
| 45-60 min. |  |  | 40 | 8 |  |  | 79 | 140 | 13 |  | 92 |  | 372 |
| Total | - | - | 166 | 44 | - | - | 254 | 581 | 45 | - | 418 | - | 1508 |
| Downstream Intersection Peak 15-min Volume: Downstream Intersection PHF: |  |  |  |  |  |  |  |  |  |  |  |  | 408 |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 0.92 |

## Heavy Vehicle Percentage Calculations

Direction: Northbound

| Source Intersection Traffic Volumes |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 60-min. Volume | EB |  |  | WB |  |  | NB |  |  | SB |  |  | Total |
|  | L | T | R | L | T | R | L | T | R | L | T | R |  |
| Total | - | - | 166 | 44 | - | - | 254 | 581 | 45 | - | 418 | - | 1508 |
| Heavy Vehicles |  |  | 1 | 1 |  |  | 3 | 8 | 1 |  | 7 |  | 21 |
|  | - | - | 0.6\% | 2.3\% | - | - | 1.2\% | 1.4\% | 2.2\% | - | 1.7\% | - |  |
|  |  |  |  |  |  |  |  |  |  |  | HV \% | 1.4\% |  |

Direction: Southbound

| Source Intersection Traffic Volumes |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 60-min. Volume | EB |  |  | WB |  |  | NB |  |  | SB |  |  | Total |
|  | L | T | R | L | T | R | L | T | R | L | T | R |  |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Heavy Vehicles |  |  |  |  |  |  |  |  |  |  |  |  | - |
|  | - | - | - | - | - | - | - | - | - | - | - | - |  |
|  |  |  |  |  |  |  |  |  |  |  | HV \% | - |  |



Peak Hour Factor Calculation

| Source Intersection Traffic Volumes |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interval | EB |  |  | WB |  |  | NB |  |  | SB |  |  | Total |
|  | L | T | R | L | T | R | L | T | R | L | T | R |  |
| 0-15 min. |  |  | 49 | 13 |  |  | 57 | 139 | 11 |  | 142 |  | 411 |
| $15-30 \mathrm{~min}$. |  |  | 49 | 14 |  |  | 56 | 129 | 7 |  | 119 |  | 374 |
| 30-45 min. |  |  | 35 | 8 |  |  | 44 | 136 | 11 |  | 124 |  | 358 |
| 45-60 min. |  |  | 53 | 12 |  |  | 56 | 149 | 8 |  | 137 |  | 415 |
| Total | - | - | 186 | 47 | - | - | 213 | 553 | 37 | - | 522 | - | 1558 |
| Downstream Intersection Peak 15-min Volume: Downstream Intersection PHF: |  |  |  |  |  |  |  |  |  |  |  |  | 415 |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 0.94 |

## Heavy Vehicle Percentage Calculations

Direction: Northbound

| Source Intersection Traffic Volumes |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 60-min. Volume | EB |  |  | WB |  |  | NB |  |  | SB |  |  | Total |
|  | L | T | R | L | T | R | L | T | R | L | T | R |  |
| Total | - | - | 186 | - | - | - | 213 | 553 | - | - | 522 | - | 1474 |
| Heavy Vehicles |  |  | 3 |  |  |  | 2 | 3 |  |  | 3 |  | 11 |
|  | - | - | 1.6\% | - | - | - | 0.9\% | 0.5\% | - | - | 0.6\% | - |  |
|  |  |  |  |  |  |  |  |  |  |  | HV \% | 0.7\% |  |

Direction: Southbound

| Source Intersection Traffic Volumes |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 60-min. Volume | EB |  |  | WB |  |  | NB |  |  | SB |  |  | Total |
|  | L | T | R | L | T | R | L | T | R | L | T | R |  |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Heavy Vehicles |  |  |  |  |  |  |  |  |  |  |  |  | - |
|  | - | - | - | - | - | - | - | - | - | - | - | - |  |
|  |  |  |  |  |  |  |  |  |  |  | HV | - |  |



Peak Hour Factor Calculation

| Source Intersection Traffic Volumes |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interval | EB |  |  | WB |  |  | NB |  |  | SB |  |  | Total |
|  | L | T | R | L | T | R | L | T | R | L | T | R |  |
| 0-15 min. | 17 | 50 | 40 |  | 91 |  | 61 |  |  |  |  | 23 | 282 |
| $15-30 \mathrm{~min}$. | 17 | 78 | 39 |  | 100 |  | 49 |  |  |  |  | 14 | 297 |
| 30-45 min. | 11 | 68 | 47 |  | 71 |  | 65 |  |  |  |  | 14 | 276 |
| 45-60 min. | 24 | 63 | 40 |  | 79 |  | 79 |  |  |  |  | 20 | 305 |
| Total | 69 | 259 | 166 | - | 341 | - | 254 | - | - | - | - | 71 | 1160 |
| Downstream Intersection Peak 15-min Volume: Downstream Intersection PHF: |  |  |  |  |  |  |  |  |  |  |  |  | 305 |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 0.95 |

## Heavy Vehicle Percentage Calculations

Direction: Northbound

| Source Intersection Traffic Volumes |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 60-min. Volume | EB |  |  | WB |  |  | NB |  |  | SB |  |  | Total |
|  | L | T | R | L | T | R | L | T | R | L | T | R |  |
| Total | 69 | 259 | 166 | - | 341 | - | 254 | - | - | - | - | 71 | 1160 |
| Heavy Vehicles | 1 | 9 | 1 |  | 4 |  | 3 |  |  |  |  | 1 | 19 |
|  | 1.4\% | 3.5\% | 0.6\% | - | 1.2\% | - | 1.2\% | - | - | - | - | 1.4\% |  |
|  |  |  |  |  |  |  |  |  |  |  | HV \% | 1.6\% |  |

Direction: Southbound

| Source Intersection Traffic Volumes |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 60-min. Volume | EB |  |  | WB |  |  | NB |  |  | SB |  |  | Total |
|  | L | T | R | L | T | R | L | T | R | L | T | R |  |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Heavy Vehicles |  |  |  |  |  |  |  |  |  |  |  |  | - |
|  | - | - | - | - | - | - | - | - | - | - | - | - |  |
|  |  |  |  |  |  |  |  |  |  |  | HV \% | - |  |



Peak Hour Factor Calculation

| Source Intersection Traffic Volumes |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interval | EB |  |  | WB |  |  | NB |  |  | SB |  |  | Total |
|  | L | T | R | L | T | R | L | T | R | L | T | R |  |
| 0-15 min. | 19 | 35 | 49 |  | 38 |  | 57 |  |  |  |  | 19 | 217 |
| $15-30 \mathrm{~min}$. | 20 | 54 | 49 |  | 46 |  | 56 |  |  |  |  | 4 | 229 |
| 30-45 min. | 22 | 64 | 35 |  | 43 |  | 44 |  |  |  |  | 22 | 230 |
| 45-60 min. | 12 | 48 | 53 |  | 46 |  | 56 |  |  |  |  | 16 | 231 |
| Total | 73 | 201 | 186 | - | 173 | - | 213 | - | - | - | - | 61 | 907 |
| Downstream Intersection Peak 15-min Volume: Downstream Intersection PHF: |  |  |  |  |  |  |  |  |  |  |  |  | 231 |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 0.98 |

## Heavy Vehicle Percentage Calculations

Direction: Northbound

| Source Intersection Traffic Volumes |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 60-min. Volume | EB |  |  | WB |  |  | NB |  |  | SB |  |  | Total |
|  | L | T | R | L | T | R | L | T | R | L | T | R |  |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Heavy Vehicles |  |  |  |  |  |  |  |  |  |  |  |  | - |
|  | - | - | - | - | - | - | - | - | - | - | - | - |  |
|  |  |  |  |  |  |  |  |  |  |  | HV \% | - |  |

Direction: Southbound

| Source Intersection Traffic Volumes |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 60-min. Volume | EB |  |  | WB |  |  | NB |  |  | SB |  |  | Total |
|  | L | T | R | L | T | R | L | T | R | L | T | R |  |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Heavy Vehicles |  |  |  |  |  |  |  |  |  |  |  |  | - |
|  | - | - | - | - | - | - | - | - | - | - | - | - |  |
|  |  |  |  |  |  |  |  |  |  |  | HV \% | - |  |



STATE OF NEW YORK - DEPARTMENT OF TRANSPORTATION
TRAFEIC AND SAEETY DIVISION
TRAFFIC CONTROL SIGNAL SPECIFICATIONS (CONTINUED)
stuay:
Contract:
PIN:
Filc:

| 43 | Orange | 4-26.93 | PAGE _ 3 - OF 19 PaGES |
| :---: | :---: | :---: | :---: |
| SIGNAL NO(S). | COUNTY | date |  |



| Phase Times [1.1.1] |  |  |  |  |  |  |  |  | Coordination Patterns [2.4] and Coordination Split Tables [2.7.1] |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | STD8 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | Pater Cyc | Of | Spit | Sed | Paf | Cyc | Off | Split | Seq | Pata | Cyc |  |  | Seq |  |  |  |  |  |  |  |  |
| Min Green | 2 | 2 | 2 |  | 2 | 2 |  |  | 10 | 0 | 1 | 4 | 13 | - | - | 13 | 1 | 25 | 0 | 0 | 0 | 1 | 37 | 0 | 0 | 0 |  |  |  |  |
| Gap, Ext | 2 | 2 | 2 |  | 2 | 2 |  |  | 2 | 0 | 2 | 4 | 14 | 0 | 0 | 14 | 1 | 26 | 0 | 0 | 0 | 1 | 38 | 0 | 0 | 0 | 1 |  |  |  |
| Max 1 | 40 | 15 | 40 |  | 40 | 15 |  |  | 3 |  | 3 | 1 | 15 | 0 | 0 | 15 | 1 | 27 | 0 | 0 | 0 | 1 | 39 | 0 | 0 | 0 | 1 |  |  |  |
| Max 2 |  |  |  |  |  |  |  |  | 4 |  | 4 | 1 | 16 | 0 | 0 | 16 | 1 | 28 | 0 | 0 | 0 | 1 | 40 | 0 | 0 | 0 | 1 | Ring/Startup [1.1.4] |  |  |
| Yel Clearance | 4 | 4 | 4 |  | 4 | 4 |  |  | 5 |  | 5 | 1 | 17 | 0 | 0 | 17 | 1 | 29 | 0 | 0 | 0 | 1 | 41 | 0 | 0 | 0 | 1 | Phs Ring | Start | Enable |
| Red Cearance | 1 | 1 | 1 |  | 1 | 1 |  |  | 6 |  | 6 | 1 | 18 | 0 | 0 | 18 | 1 | 30 | 0 | 0 | 0 | 1 | 42 | 0 | 0 | 0 | 1 | T | GREEN | On |
| Walk |  |  |  |  |  |  |  |  | 7 |  | 7 | 1 | 19 | 0 | 0 | 19 | 1 | 31 | 0 | 0 | 0 | 1 | 43 | 0 | 0 | 0 | 1 | , | RED | On |
| Ped Clearance |  |  |  |  |  |  |  |  | 8 |  | 8 | 1 | 20 | 0 | 0 | 20 | 1 | 32 | 0 | 0 | 0 | 1 | 44 | 0 | 0 | 0 | 1 | 31 | RED | On |
| Red Revert |  |  |  |  |  |  |  |  | 9 |  | 9 | 1 | 21 | 0 | 0 | 21 | 1 | 33 | 0 | 0 | 0 | 1 | 45 | 0 | 0 | 0 | 1 | 41 | RED | Off |
| Adc Initial |  |  |  |  |  |  |  |  | 10 |  | 10 | 1 | 22 | 0 | 0 | 22 | 1 | 34 | 0 | 0 | 0 | 1 | 46 | 0 | 0 | 0 | 1 | 5 2 | GREEN | On |
| Max Initial |  |  |  |  |  |  |  |  | 11 |  | 11 | 1 | 23 | 0 | 0 | 23 | 1 | 35 | 0 | 0 | 0 | 1 | 47 | 0 | 0 | 0 | 1 | $6{ }^{6}$ | RED | On |
| Time B4 Reduct |  |  |  |  |  |  |  |  | 12 |  | 12 | 1 | 24 | 0 | 0 | 24 | 1 | 36 | 0 | 0 | 0 | 1 | 48 | 0 | 0 | 0 | 1 | 72 | RED | Off |
| Cars 54 Reduct |  |  |  |  |  |  |  |  | Solit | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | Split |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 2 | RED | Off |
| Time To Reduce |  |  |  |  |  |  |  |  | 1 Coor | 40 | 15 | 40 |  | 40 | 15 |  |  | ${ }^{13}$ | Coor | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Coord Modes [2.1] |  |  |
| Reduce By |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | NON | NON | NON | NON | NON | NON | NON | NON | Test OFMoce | 0 |  |
| Min Gap |  |  |  |  |  |  |  |  | 2 Coor | 60 | 15 | 40 |  | 60 | 15 |  |  | 14 | Coor | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Correction | SHRT/LNG |  |
| DyMaxLm |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | NON | NON | NON | NON | NON | NON | NON | NON | Maximum | MAX 1 |  |
| Max Steo |  |  |  |  |  |  |  |  | Coor |  |  |  |  |  |  |  |  | 15 | Coor | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Force-Off | FLOAT |  |
| Options [1.1.2] | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |  |  |  |  |  |  |  | NON | NON | NON | NON | NON | NON | NON | NON | Closed LCop | ON |  |
| Enable | On | On | On |  | On | On |  |  | Coor |  |  |  |  |  |  |  |  | 16 | Coor | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | Stop-in-Walk | OFF |  |
| Min Recall | On |  |  |  | On |  |  |  |  |  |  |  |  |  |  |  |  |  |  | NON | NON | NON | NON | NON | NON | NON | NON | Auto Reset | ON |  |
| Max Recall |  |  |  |  |  |  |  |  | 5 Coor |  |  |  |  |  |  |  |  | 17 | Coor | 0 | C | 0 | 0 | 0 | 0 | 0 | - | Expand Splt | OFF |  |
| Ped Recall |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | NON | NON | NON | NON | NON | NON | NON | NON | Pec Recyce | NO_RECYCLE |  |
| Soft Recall |  |  |  |  |  |  |  |  | 6 Coor |  |  |  |  |  |  |  |  | 18 | Coor | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Before | TIMED |  |
| Lock Calls |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | NON | NON | NON | NON | NON | NON | NON | NON | After | TIMED |  |
| Auto Flast Entry |  |  |  |  |  |  |  |  | Coor |  |  |  |  |  |  |  |  | 19 | Coor | , | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Auto Flash [ | [1.4.1] |  |
| Auto Flash Ext |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | NON | NON | NON | NON | NON | NON | NON | NON | Auto Flash | PH OVER |  |
| Dual Entry |  | On |  | On |  | On |  | On | 8 Coor |  |  |  |  |  |  |  |  | 20 | Coor | 0 | 0 | C | 0 | 0 | 0 | 0 | - | Flash Yel | 45 |  |
| Enable Simul Gap | On | On | On | On | On | On | On | On |  |  |  |  |  |  |  |  |  |  |  | NON | NON | NON | NON | NON | NON | NON | NON | Flash Red | 0 |  |
| Gaurantee Passag |  |  |  |  |  |  |  |  | 9 Ccor |  |  |  |  |  |  |  |  | 21 | Coor | 0 | O | 0 | 0 | 0 | 0 | 0 | 0 | Unit Params [1.2.1] |  |  |
| Rest In Walk |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | NON | NON | NON | NON | NON | NON | NON | NON | Phase Mode | STD8 |  |
| Conditon Service |  |  |  |  |  |  |  |  | 10 Ccor |  |  |  |  |  |  |  |  | 22 | Coor | , | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | USER |  |
| Non-Actuated 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | NON | NON | NON | NON | NON | NON | NON | NON | 10 Mode | ON |  |
| Non-Actuated 2 |  |  |  |  |  |  |  |  | 11 Coor |  |  |  |  |  |  |  |  | 23 | Coor | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Start Fash(s) <br> Start AllRed(s) | 0 |  |
| Add int Calc |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | NON | NON | NON | NON | NON | NON | NON | NON |  | 0 |  |
| Options+ [1.1.3] | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 12 Coor |  |  |  |  |  |  |  |  | 24 | Coor | 0 | 0 | 0 | 0 | - | , | , | 0 | Yellow < 3" | OFF |  |
| Reservice |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | NON | NON | NON | NON | NON | NON | NON | NON |  | 20 |  |
| PedClit Thru Yel |  |  |  |  |  |  |  |  | Page\# |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 |  |
| Skip Red No Call |  |  |  |  |  |  |  |  | 1 | 8 Ph | hase T | Time | s/Op | lions; | Patt | erns/S | plits; | Ring | g Sta | tartup; | C00 | ord/Fl | lash M | Mode | Unit $F$ | Param |  | $\frac{\text { Red Revert }}{\text { MCE Timeout }}$ | 0 |  |
| Rec Rest |  |  |  |  |  |  |  |  | 1A\&1B | 16 Ph | hase 7 | Time | s/Op | tions; | Patt | Cerns/S | pplit; | Ring | g Sta | tartup; | Coor | ord/Fl | lash M | Mode | Unit $F$ | Param |  | Feature Profie | 0 |  |
| Mex II |  |  |  |  |  |  |  |  | 2 | Overla | laps; | Cha | nel | Setin | gs; | Coord | At T | able+ | + [val | alues n | not as | ssocia | ated $w$ | with tim | me-of- | -day) |  | Free Ring Sea | 1 |  |
| Call Phase |  |  |  |  |  |  |  |  | 3 | Detec | ction; | San | mple | Time | and 1 | Unit Pa | ame | eters | reate | ted to | detec | ection |  |  |  |  |  | Auxswitch | STOPTM |  |
| Conflicting Phase |  |  |  |  |  |  |  |  | 4 P | Preem | mption | n and | d Alte | rnate | Phas | se Tim | e ard | d Ph | ase 0 | Option |  |  |  |  |  |  |  | SDLC Retry | 0 |  |
| Onit Yellow |  |  |  |  |  |  |  |  | 5 A | Arnua | a Sch | hedul |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | TS2 Det Faults | ON |  |
| Ped Deay |  |  |  |  |  |  |  |  | 6 | Day P | Plans; | ; Actio | On Ta | ables; | Coo | ord Alt | Tab | ${ }^{+}$( | values | es vari | ied by | y time | e-of-da |  |  |  |  | Auto Ped Clear | OFF |  |
| Gri/Ped Delay |  |  |  |  |  |  |  |  | 7 C | Communications; Secutiry; l/O Setup |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | SELC Retry | Page 1 |  |
| ID: 3043 RTE 52 @ UNION AVE (RTE 300) |  |  |  |  |  |  |  |  | 8 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Cole Rety |  |  |








|  | $\cdots$ | $G$ | A | $\omega$ | N | $\rightarrow$ | 菏 | O | $G$ | － | $\omega$ | N | $\rightarrow$ | －${ }_{\text {O }}^{\text {® }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\frac{7}{2}$ |  |  |  |  |  |  | $\begin{aligned} & \pi \\ & \mathbb{D} \end{aligned}$ |  |  |  |  |  |  | 高 |
| $\begin{aligned} & \overrightarrow{\mathbf{R}} \\ & \stackrel{\rightharpoonup}{0} \\ & \underset{3}{3} \\ & \stackrel{8}{6} \end{aligned}$ |  |  |  |  |  |  | $\left\lvert\, \begin{aligned} & \underline{0} \\ & \stackrel{0}{\mathbb{D}} \\ & \frac{1}{3} \end{aligned}\right.$ | N | N | N | N | N | N | 3 $\vdots$ $\square$ $\sum$ § |
|  | $0$ | 우 | 운 | $\begin{aligned} & 0 \\ & 11 \\ & 11 \end{aligned}$ | $\begin{aligned} & 0 \\ & 11 \\ & \hline 1 \end{aligned}$ | $\frac{0}{11}$ | $\frac{\infty}{\frac{\pi}{0}}$ |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1 <br> 0 <br> 8 <br> 8 <br> 1 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | ¢ |




| $\rightarrow$ | $\begin{aligned} & \underset{\vec{\nabla}}{\mathbf{D}} \\ & \# \\ & \# \end{aligned}$ | $\infty$ | $G$ | － | $\omega$ | N | ， | O ® \＃ \＃ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\frac{2}{2}$ | $\frac{2}{2}$ | $\frac{0}{2}$ | $\frac{0}{2}$ | $10$ | $\frac{0}{2}$ |  |
|  | $\begin{aligned} & \vdots \\ & \stackrel{\zeta}{3} \end{aligned}$ |  | $\begin{aligned} & m \\ & \frac{\pi}{2} \\ & m \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & m \\ & \frac{m}{3} \\ & m \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & m \\ & m \\ & \pi \\ & \hline \pi \end{aligned}$ | 召 | 召 | 守 |
|  | $\frac{\text { 늧 }}{\sum}$ | $\begin{aligned} & 0 \\ & \frac{8}{m} \\ & \Gamma \\ & \hline \end{aligned}$ | $\begin{aligned} & \frac{0}{2} \\ & \Gamma \\ & \Gamma \end{aligned}$ | $\begin{aligned} & 0 \\ & \frac{0}{3} \\ & \pi \\ & \Gamma \\ & \hline \end{aligned}$ | $\begin{aligned} & \frac{0}{2} \\ & \frac{1 \pi}{2} \\ & \hline \end{aligned}$ | $\begin{aligned} & 0 \\ & \frac{8}{\pi} \\ & \Gamma \\ & \hline \end{aligned}$ |  | $\begin{aligned} & 0 \\ & \stackrel{y}{7} \\ & \underset{\sim}{5} \end{aligned}$ |
|  |  |  |  |  |  |  |  | 号 |
| $2$ | $\begin{aligned} & 8 \\ & 0 \\ & + \\ & 0 \\ & \mathbf{0} \end{aligned}$ |  |  |  |  |  |  | § |














## 





| $\begin{array}{\|c} 0 \\ \infty \\ \vdots \\ \infty \end{array}$ |  | $\begin{array}{l\|l} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{array}$ | $\left\|\begin{array}{c} 0 \\ 0 \\ 0 \\ 0 \end{array}\right\|$ | $\begin{array}{\|c\|c\|} \hline 0 & 0 \\ 0 \\ 0 \\ \vdots \end{array}$ | $\left\lvert\, \begin{gathered} 0 \\ 0 \\ 0 \\ \omega \\ \hline \end{gathered}\right.$ | $0 \begin{gathered} 0 \\ 0 \\ 0 \\ 0 \\ N \end{gathered}$ | $\begin{aligned} & 0 \\ & 0 \\ & 1 \\ & 1 \end{aligned}$ | $\frac{?}{\stackrel{\rightharpoonup}{9}}$ | ¢ | $\bigcirc$ | 人 | 安 | $\left\|\begin{array}{c} \stackrel{+}{\infty} \\ + \end{array}\right\|$ | $\left\|\begin{array}{c} \stackrel{8}{\infty} \\ \dot{\omega} \end{array}\right\|$ | $\left\|\begin{array}{c} \overline{9} \\ i \end{array}\right\|$ | － | $\left\|\begin{array}{c} -7 \\ \infty \\ \infty \end{array}\right\|$ | $\begin{gathered} - \\ \vdots \\ \vdots \end{gathered}$ | $\begin{array}{\|c\|} \hline-\bar{j} \\ \dot{\alpha} \end{array}$ | － | $\left\lvert\, \begin{gathered} -3 \\ -8 \end{gathered}\right.$ | $\left\lvert\, \begin{gathered} \underset{\sim}{\omega} \\ \stackrel{y}{2} \end{gathered}\right.$ | $\left\|\begin{array}{c} -3 \\ \vdots \\ i \end{array}\right\|$ | － | $\stackrel{\stackrel{\rightharpoonup}{A}}{\stackrel{+}{2}}$ | $\mid \underset{\dot{\omega}}{\stackrel{\rightharpoonup}{*}}$ | 交 | $\stackrel{\text { ¢ }}{\stackrel{1}{-}}$ | $\stackrel{?}{\stackrel{\rightharpoonup}{e}}$ | O | $\left\|\begin{array}{l} 0 \\ 1 \\ 1 \end{array}\right\|$ | $\left\|\begin{array}{l} 0 \\ 0 \\ 0 \\ 0 \end{array}\right\|$ | $\begin{array}{\|c} 0 \\ 0 \\ 3 \\ \hline \end{array}$ | $\left\|\begin{array}{c} 0 \\ 1 \\ 1 \end{array}\right\|$ | O | 足 |  | $\frac{\square}{1}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|l\|l} \hline \stackrel{\rightharpoonup}{u} \\ \hline \end{array}$ | $\stackrel{\rightharpoonup}{n} \stackrel{\rightharpoonup}{\mathrm{r}}$ | $\stackrel{\rightharpoonup}{\vec{v}}$ | $\|\stackrel{\rightharpoonup}{\vec{v}}\|$ | $\begin{array}{l\|l} \vec{~} & \vec{\rightharpoonup} \\ \hline \end{array}$ | $\begin{array}{\|l\|l\|} \hline \stackrel{\rightharpoonup}{c} \\ \hline \end{array}$ | $\begin{array}{\|l\|l\|} \hline \stackrel{\rightharpoonup}{n} \\ \hline \end{array}$ |  | coc | $\left\lvert\, \begin{aligned} & \vec{\infty} \\ & \substack{ \\ \hline} \\ & \hline \end{aligned}\right.$ | $\begin{array}{\|l\|l\|} \hline \infty \\ \hline \end{array}$ | $\begin{array}{\|c\|} \hline \stackrel{\infty}{\infty} \\ \hline \end{array}$ | $\begin{array}{\|c\|} \hline \stackrel{\rightharpoonup}{\infty} \\ \hline \end{array}$ | $\begin{array}{\|l\|l\|} \hline \infty \\ 0 \\ \hline \end{array}$ | $\begin{array}{\|l\|} \hline \infty \\ \infty \\ \hline \end{array}$ | $\left\|\begin{array}{l} \vec{\infty} \\ \infty \end{array}\right\|$ | $\left\|\begin{array}{c} \vec{\infty} \\ 0 \end{array}\right\|$ | $\begin{array}{\|c\|} \hline \stackrel{\infty}{\infty} \\ \hline \end{array}$ | $\begin{array}{\|l\|} \hline \\ \mathbf{o} \\ \hline \end{array}$ | $\begin{array}{\|c\|} \hline \\ \infty \\ \hline \end{array}$ | $\left.\begin{array}{\|c} \stackrel{\rightharpoonup}{\infty} \\ \infty \end{array} \right\rvert\,$ | $\stackrel{\rightharpoonup}{0}$ | $\begin{array}{\|c\|} \hline \stackrel{\infty}{\infty} \\ \hline \end{array}$ | $\begin{array}{\|c\|} \hline \stackrel{\rightharpoonup}{\infty} \\ \hline \end{array}$ | $\begin{array}{\|c\|} \hline \\ \infty \\ \hline \end{array}$ | $\begin{array}{\|c\|} \vec{\infty} \\ \mathbf{o} \\ \hline \end{array}$ | $\stackrel{\rightharpoonup}{\infty}$ | $\begin{array}{\|l\|} \hline \infty \\ \infty \\ \hline \end{array}$ | $\begin{array}{\|l\|} \stackrel{\infty}{\infty} \\ \hline \end{array}$ |  | $\stackrel{\rightharpoonup}{\mathrm{r}}$ | $\mid \vec{~}$ | $\stackrel{\rightharpoonup}{\mathrm{a}}$ | $\stackrel{\rightharpoonup}{\mathrm{u}}$ | $\stackrel{\rightharpoonup}{\mathrm{v}}$ | $\stackrel{\rightharpoonup}{\vec{*}}$ | $\stackrel{\rightharpoonup}{\text { ज }}$ |  | ज |
|  | $\mathfrak{c}$ |  | $\left.\begin{array}{\|c\|} \hline \mathbf{z} \\ \underset{\sim}{C} \\ c \\ \underset{O}{2} \end{array} \right\rvert\,$ |  |  |  |  |  | $\left\|\begin{array}{l} \stackrel{c}{c} \\ \stackrel{c}{\hat{N}} \\ \stackrel{\rightharpoonup}{\alpha} \end{array}\right\|$ |  |  |  |  |  |  |  |  | $\square$ | $\square$ | $\square$ |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \hline \underset{\sim}{z} \\ & \underset{\sim}{c} \\ & \underset{\otimes}{\otimes} \end{aligned}$ |  |  | $\left.\begin{aligned} & \underset{\sim}{z} \\ & \underset{\sim}{c} \\ & \underset{\sim}{Q} \end{aligned} \right\rvert\,$ |  | $\left.\begin{aligned} & \underset{z}{z} \\ & \underset{\sim}{c} \\ & \underset{\sim}{w} \end{aligned} \right\rvert\,$ | $\left\lvert\, \begin{aligned} & \underset{\sim}{z} \\ & \underset{\sim}{\dot{N}} \\ & \dot{\otimes} \end{aligned}\right.$ | 年 |



TAPS STUDY \#
FILE \#
PAGE 17 OF 19

SIGNAL \#
COUNTY \# DranOR DATE $\frac{4-26-93}{\text { TABLE OF SWITCH PACKS }}$


```
Land Use Code: 934 Fast-Food Restaurant with Drive-Through Window
Setting: General Urban/Suburban
Size: 2.342
AMC
11/8/2022
1021-22-01537
```

ITE Study Information

| Peak Hour |
| :--- |
| Weekday |
| AM Peak Street Hour |
| PM Peak Street Hour |
| AM Generator |
| PM Generator |
| Saturday |
| Saturday Generator |
| Sunday |
| Sunday Generator |


| \# Studies | Avg. <br> Variable |
| :---: | :---: |
| 71 | 3 |
| 96 | 4 |
| 190 | 3 |
| 118 | 3 |
| 135 | 3 |
| 17 | 3 |
| 53 | 4 |
| 15 | 3 |
| 10 | 3 |


| Distribution |  |
| :---: | :---: |
| In | Out |
| $50 \%$ | $50 \%$ |
| $51 \%$ | $49 \%$ |
| $52 \%$ | $48 \%$ |
| $52 \%$ | $48 \%$ |
| $51 \%$ | $49 \%$ |
| $50 \%$ | $50 \%$ |
| $51 \%$ | $49 \%$ |
| $50 \%$ | $50 \%$ |
| $48 \%$ | $52 \%$ |

Trip Generation using ITE Average Rates

| Peak Hour | Rate |  |  |  | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Min. | Avg. | Max. | S.D. | In | Out | Total |
| Weekday | 98.89 | 467.48 | 1137.66 | 238.62 | 548 | 547 | 1095 |
| AM Peak Street Hour | 1.05 | 44.61 | 164.25 | 27.14 | 53 | 51 | 104 |
| PM Peak Street Hour | 8.77 | 33.03 | 117.22 | 17.59 | 40 | 37 | 77 |
| AM Generator | 7.28 | 50.57 | 164.25 | 25.99 | 61 | 57 | 118 |
| PM Generator | 13.36 | 50.94 | 159.07 | 24.91 | 61 | 58 | 119 |
| Saturday | 218.91 | 616.12 | 1410.88 | 320.90 | 722 | 721 | 1443 |
| Saturday Generator | 11.25 | 55.25 | 122.92 | 24.62 | 66 | 63 | 129 |
| Sunday | 213.45 | 472.58 | 953.97 | 215.31 | 554 | 553 | 1107 |
| Sunday Generator | 26.55 | 55.15 | 98.15 | 23.88 | 62 | 67 | 129 |

Trip Generation using ITE Equations

| Peak Hour | Equation | $\mathrm{R}^{2}$ value | Effective Rate | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | In | Out | Total |
| Weekday | Not Given |  | - |  |  |  |
| AM Peak Street Hour | Not Given |  | - |  |  |  |
| PM Peak Street Hour | Not Given |  | - |  |  |  |
| AM Generator | Not Given |  | - |  |  |  |
| PM Generator | Not Given |  | - |  |  |  |
| Saturday | Not Given |  | - |  |  | - |
| Saturday Generator | Not Given |  | - |  |  |  |
| Sunday | Not Given |  | - |  |  |  |
| Sunday Generator | Not Given |  | - |  |  |  |

ITE Land Use Subcategory Description and/or DTraffic Comments:

Land Use Code: 934 Fast-Food Restaurant with Drive-Through Window
Setting:
Size:
Prepared By:
Date:
Job \#:

## General Urban/Suburban

2.342 KSF

AMC
11/8/2022
1021-22-01537

Calculation of Passby Trips

| Trip Type | Passby$\%$ | Trip Generation |  |  | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | In | Out | Total | In | Out |  |


| ak Street Hour |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total | 50\% | x | 53 | 51 | 104 | - | - |  |
| Passby |  |  | 27 | 25 | 52 | - | - |  |
| New (Primary) |  |  | 26 | 26 | 52 | - |  |  |


| Peak Street Hour |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total | 55\% | x | 40 | 37 | 77 | - | - |  |
| Passby |  |  | 22 | 20 | 42 | - | - | - |
| New (Primary) |  |  | 18 | 17 | 35 | - | - |  |


| AM Generator |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total | 50\% | x | 61 | 57 | 118 | - | - |  |
| Passby |  |  | 31 | 28 | 59 | - | - |  |
| New (Primary) |  |  | 30 | 29 | 59 | - |  |  |


| enerator |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total | 55\% | $x$ | 61 | 58 | 119 | - | - |  |
| Passby |  |  | 34 | 31 | 65 | - | - |  |
| New (Primary) |  |  | 27 | 27 | 54 | - | - |  |


| Saturday Generator |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total | 50\% | $x$ | 66 | 63 | 129 | - |  |
| Passby |  |  | 33 | 32 | 65 | - |  |
| New (Primary) |  |  | 33 | 31 | 64 | - |  |

Passby Comments: Saturday peak hour passby \% approved by NJDOT.

```
Land Use Code: 934 Fast-Food Restaurant with Drive-Through Window
Setting: General Urban/Suburban
Size:
Prepared By:
Date: 11/8/2022
Job #: 1021-22-01537
```

ITE Study Information

| Peak Hour |
| :--- |
| Weekday |
| AM Peak Street Hour |
| PM Peak Street Hour |
| AM Generator |
| PM Generator |
| Saturday |
| Saturday Generator |
| Sunday |
| Sunday Generator |


| \# | Avg. |
| ---: | ---: |
| Studies |  | Variable | 71 | 3 |
| ---: | ---: |
| 96 | 4 |
| 190 | 3 |
| 118 | 3 |
| 135 | 3 |
| 17 | 3 |
| 53 | 4 |
| 15 | 3 |
| 10 | 3 |


| Distribution |  |
| :---: | :---: |
| In | Out |
| $50 \%$ | $50 \%$ |
| $51 \%$ | $49 \%$ |
| $52 \%$ | $48 \%$ |
| $52 \%$ | $48 \%$ |
| $51 \%$ | $49 \%$ |
| $50 \%$ | $50 \%$ |
| $51 \%$ | $49 \%$ |
| $50 \%$ | $50 \%$ |
| $48 \%$ | $52 \%$ |

Trip Generation using ITE Average Rates

| Peak Hour | Rate |  |  |  | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Min. | Avg. | Max. | S.D. | In | Out | Total |
| Weekday | 98.89 | 467.48 | 1137.66 | 238.62 | 593 | 593 | 1186 |
| AM Peak Street Hour | 1.05 | 44.61 | 164.25 | 27.14 | 58 | 55 | 113 |
| PM Peak Street Hour | 8.77 | 33.03 | 117.22 | 17.59 | 44 | 40 | 84 |
| AM Generator | 7.28 | 50.57 | 164.25 | 25.99 | 67 | 61 | 128 |
| PM Generator | 13.36 | 50.94 | 159.07 | 24.91 | 66 | 63 | 129 |
| Saturday | 218.91 | 616.12 | 1410.88 | 320.90 | 782 | 781 | 1563 |
| Saturday Generator | 11.25 | 55.25 | 122.92 | 24.62 | 71 | 69 | 140 |
| Sunday | 213.45 | 472.58 | 953.97 | 215.31 | 600 | 599 | 1199 |
| Sunday Generator | 26.55 | 55.15 | 98.15 | 23.88 | 67 | 73 | 140 |

Trip Generation using ITE Equations

| Peak Hour | Equation | $\mathrm{R}^{2}$ value | Effective Rate | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | In | Out | Total |
| Weekday | Not Given |  | - |  |  |  |
| AM Peak Street Hour | Not Given |  | - |  |  |  |
| PM Peak Street Hour | Not Given |  | - |  |  |  |
| AM Generator | Not Given |  | - |  |  | - |
| PM Generator | Not Given |  | - |  |  | - |
| Saturday | Not Given |  | - |  |  | - |
| Saturday Generator | Not Given |  | - |  |  | - |
| Sunday | Not Given |  | - |  |  | - |
| Sunday Generator | Not Given |  | - |  |  | - |

ITE Land Use Subcategory Description and/or DTraffic Comments:

Land Use Code: 934 Fast-Food Restaurant with Drive-Through Window
Setting:
Size:
Prepared By:
Date:
Job \#:

## General Urban/Suburban

2.537 KSF

AMC
11/8/2022
1021-22-01537

Calculation of Passby Trips

| ip Type | Passby$\%$ | Trip Generation |  |  | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Trip Type |  | In | Out | Total | In | Out | To |


| ak Street Hour |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total | 50\% | x | 58 | 55 | 113 | - | - |  |
| Passby |  |  | 29 | 28 | 57 | - | - |  |
| New (Primary) |  |  | 29 | 27 | 56 | - |  |  |


| eak Street Hour |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total | 55\% | x | 44 | 40 | 84 | - | - |  |
| Passby |  |  | 24 | 22 | 46 | - | - | - |
| New (Primary) |  |  | 20 | 18 | 38 | - | - |  |

AM Generator

| Total | 50\% | $x$ | 67 | 61 | 128 | - | - |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Passby |  |  | 34 | 30 | 64 | - | - |  |
| New (Primary) |  |  | 33 | 31 | 64 | - | - |  |


| enerator |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total | 55\% | x | 66 | 63 | 129 | - | - |  |
| Passby |  |  | 36 | 35 | 71 | - | - |  |
| New (Primary) |  |  | 30 | 28 | 58 | - | - |  |


| Saturday Generator |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total | 50\% | $x$ | 71 | 69 | 140 | - |  |
| Passby |  |  | 36 | 34 | 70 | - |  |
| New (Primary) |  |  | 35 | 35 | 70 | - |  |

Passby Comments: Saturday peak hour passby \% approved by NJDOT.

Trip Generation Worksheet, ITE Trip Generation $10^{\text {th }}$ Edition

```
Land Use Code: 220 Multifamily Housing (Low-Rise) (Dwelling Units)
Size: 246 Dwelling Units
Prepared By:
ARF
Date: 12/2/2022
Job #: 1021-22-01537
```

ITE Study Information

| Peak Hour | $\begin{gathered} \# \\ \text { Studies } \end{gathered}$ | Avg. Variable | Distribution |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | In | Out |
| Weekday | 29 | 168 | 50\% | 50\% |
| AM Peak Street Hour | 42 | 199 | 23\% | 77\% |
| PM Peak Street Hour | 50 | 187 | 63\% | 37\% |
| AM Generator | 36 | 161 | 28\% | 72\% |
| PM Generator | 35 | 146 | 59\% | 41\% |
| Saturday | 5 | 89 | 50\% | 50\% |
| Saturday Generator | 5 | 89 | 0\% | 0\% |
| Sunday | 5 | 89 | 50\% | 50\% |
| Sunday Generator | 5 | 89 |  |  |

Trip Generation using ITE Average Rates

| Peak Hour | Rate |  |  |  | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Min. | Avg. | Max. | S.D. | In | Out | Total |
| Weekday | 4.45 | 7.32 | 10.97 | 1.31 | 901 | 900 | 1801 |
| AM Peak Street Hour | 0.18 | 0.46 | 0.74 | 0.12 | 26 | 87 | 113 |
| PM Peak Street Hour | 0.18 | 0.56 | 1.25 | 0.16 | 87 | 51 | 138 |
| AM Generator | 0.34 | 0.56 | 0.97 | 0.15 | 39 | 99 | 138 |
| PM Generator | 0.41 | 0.67 | 1.25 | 0.14 | 97 | 68 | 165 |
| Saturday | 3.36 | 8.14 | 11.40 | 2.94 | 1001 | 1001 | 2002 |
| Saturday Generator | 0.41 | 0.70 | 0.93 | 0.20 |  |  | 172 |
| Sunday | 2.61 | 6.28 | 8.22 | 1.96 | 773 | 772 | 1545 |
| Sunday Generator | 0.36 | 0.67 | 0.93 | 0.22 |  |  | 165 |

Trip Generation using ITE Equations

| Peak Hour | Equation | $\mathrm{R}^{2}$ value | Effective Rate | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | In | Out | Total |
| Weekday | T = 7.56(X) - 40.86 | 0.96 | 7.39 | 910 | 909 | 1819 |
| AM Peak Street Hour | $\operatorname{Ln}(\mathrm{T})=0.95 \operatorname{Ln}(\mathrm{X})-0.51$ | 0.90 | 0.46 | 26 | 86 | 112 |
| PM Peak Street Hour | $\operatorname{Ln}(\mathrm{T})=0.89 \operatorname{Ln}(\mathrm{X})-0.02$ | 0.86 | 0.54 | 83 | 49 | 132 |
| AM Generator | $\operatorname{Ln}(\mathrm{T})=0.94 \operatorname{Ln}(\mathrm{X})-0.29$ | 0.91 | 0.54 | 37 | 95 | 132 |
| PM Generator | $\mathrm{T}=0.66(\mathrm{X})+1.41$ | 0.94 | 0.67 | 97 | 67 | 164 |
| Saturday | $\mathrm{T}=14.01(\mathrm{X})-521.69$ | 0.93 | 11.89 | 1463 | 1462 | 2925 |
| Saturday Generator | $\mathrm{T}=1.08(\mathrm{X})-33.24$ | 0.92 | 0.94 | - |  | 232 |
| Sunday | T = 10.13(X) - 341.89 | 0.96 | 8.74 | 1075 | 1075 | 2150 |
| Sunday Generator | $\mathrm{T}=1.12(\mathrm{X})-40.41$ | 0.93 | 0.96 | - |  | 235 |

DTraffic Comments: For all Weekend Trip Generation (Saturday, Saturday Generator, Sunday, Sunday Generator), use Rates if <90 Units and use Equation if >=90 Units.

| Land Use Code: | 150 Warehousing (KSF) |  |
| :--- | :--- | :--- |
| Size: | 290 | KSF |
| Prepared By: | ARF |  |
| Date: | $12 / 2 / 2022$ |  |
| Job \#: | $1021-22-01537$ |  |

ITE Study Information

| Peak Hour | \# <br> Studies | Avg. Variable | Distribution |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | In | Out |
| Weekday | 29 | 285 | 50\% | 50\% |
| AM Peak Street Hour | 34 | 451 | 77\% | 23\% |
| PM Peak Street Hour | 47 | 400 | 27\% | 73\% |
| AM Generator | 23 | 274 | 65\% | 35\% |
| PM Generator | 25 | 275 | 24\% | 76\% |
| Saturday | 3 | 226 | 50\% | 50\% |
| Saturday Generator | 2 | 129 | 64\% | 36\% |
| Sunday | 3 | 226 | 50\% | 50\% |
| Sunday Generator | 2 | 129 | 52\% | 48\% |

Trip Generation using ITE Average Rates

| Peak Hour | Rate |  |  |  | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Min. | Avg. | Max. | S.D. | In | Out | Total |
| Weekday | 0.15 | 1.74 | 16.93 | 1.55 | 253 | 252 | 505 |
| AM Peak Street Hour | 0.02 | 0.17 | 1.93 | 0.20 | 38 | 11 | 49 |
| PM Peak Street Hour | 0.01 | 0.19 | 1.80 | 0.18 | 15 | 40 | 55 |
| AM Generator | 0.02 | 0.22 | 2.08 | 0.28 | 42 | 22 | 64 |
| PM Generator | 0.02 | 0.24 | 1.80 | 0.24 | 17 | 53 | 70 |
| Saturday | 0.01 | 0.15 | 1.58 | 1.12 | 22 | 22 | 44 |
| Saturday Generator | 0.01 | 0.05 | 0.22 |  | 10 | 5 | 15 |
| Sunday | 0.03 | 0.06 | 0.32 | 0.23 | 9 | 8 | 17 |
| Sunday Generator | 0.02 | 0.04 | 0.11 |  | 6 | 6 | 12 |

Trip Generation using ITE Equations

| Peak Hour |
| :--- |
| Weekday |
| AM Peak Street Hour |
| PM Peak Street Hour |
| AM Generator |
| PM Generator |
| Saturday |
| Saturday Generator |
| Sunday |
| Sunday Generator |

DTraffic Comments: Generally accepted as warehouse if < 10\% office use \& if office use is ancillary to warehouse use

```
Land Use Code: 252 Senior Adult Housing - Multifamily
Setting: General Urban/Suburban
Size: 100.000 Dwelling Units
Prepared By:
ARF
12/2/2022
1021-22-01537
```

ITE Study Information

| Peak Hour | $\begin{gathered} \# \\ \text { Studies } \end{gathered}$ | Avg. Variable | Distribution |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | In | Out |
| Weekday | 6 | 72 | 50\% | 50\% |
| AM Peak Street Hour | 9 | 73 | 34\% | 66\% |
| PM Peak Street Hour | 9 | 73 | 56\% | 44\% |
| AM Generator | 10 | 79 | 45\% | 55\% |
| PM Generator | 10 | 79 | 54\% | 46\% |
| Saturday | 8 | 76 | 50\% | 50\% |
| Saturday Generator | 9 | 84 | 54\% | 46\% |
| Sunday | 8 | 76 | 50\% | 50\% |
| Sunday Generator | 8 | 76 | 51\% | 49\% |

Trip Generation using ITE Average Rates

| Peak Hour | Rate |  |  |  | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Min. | Avg. | Max. | S.D. | In | Out | Total |
| Weekday | 2.59 | 3.24 | 4.79 | 0.53 | 162 | 162 | 324 |
| AM Peak Street Hour | 0.13 | 0.20 | 0.27 | 0.04 | 7 | 13 | 20 |
| PM Peak Street Hour | 0.16 | 0.25 | 0.36 | 0.06 | 14 | 11 | 25 |
| AM Generator | 0.19 | 0.29 | 0.64 | 0.10 | 13 | 16 | 29 |
| PM Generator | 0.24 | 0.30 | 0.46 | 0.06 | 16 | 14 | 30 |
| Saturday | 1.84 | 2.74 | 4.07 | 0.62 | 137 | 137 | 274 |
| Saturday Generator | 0.23 | 0.32 | 0.50 | 0.09 | 17 | 15 | 32 |
| Sunday | 2.15 | 2.70 | 4.25 | 0.62 | 135 | 135 | 270 |
| Sunday Generator | 0.25 | 0.34 | 0.55 | 0.11 | 17 | 17 | 34 |

Trip Generation using ITE Equations

| Peak Hour | Equation | $\mathrm{R}^{2}$ value | Effective Rate | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | In | Out | Total |
| Weekday | $\mathrm{T}=2.89(\mathrm{X})+24.82$ | 0.99 | 3.14 | 157 | 157 | 314 |
| AM Peak Street Hour | $\mathrm{T}=0.19(\mathrm{X})+0.90$ | 0.85 | 0.20 | 7 | 13 | 20 |
| PM Peak Street Hour | $\mathrm{T}=0.25(\mathrm{X})+0.07$ | 0.84 | 0.25 | 14 | 11 | 25 |
| AM Generator | $\mathrm{T}=0.19(\mathrm{X})+8.01$ | 0.85 | 0.27 | 12 | 15 | 27 |
| PM Generator | $\mathrm{T}=0.29(\mathrm{X})+0.82$ | 0.93 | 0.30 | 16 | 14 | 30 |
| Saturday | $\mathrm{T}=2.33(\mathrm{X})+31.21$ | 0.90 | 2.64 | 132 | 132 | 264 |
| Saturday Generator | $\operatorname{Ln}(\mathrm{T})=0.93 \operatorname{Ln}(\mathrm{X})-0.81$ | 0.87 | 0.32 | 17 | 15 | 32 |
| Sunday | $\mathrm{T}=2.01(\mathrm{X})+52.51$ | 0.91 | 2.54 | 127 | 127 | 254 |
| Sunday Generator | $\operatorname{Ln}(\mathrm{T})=0.78 \operatorname{Ln}(\mathrm{X})-0.08$ | 0.80 | 0.34 | 17 | 17 | 34 |

ITE Land Use Subcategory Description and/or DTraffic Comments:

Land Use Code:
Setting:
Size:
Prepared By:
Date:
Job \#:

912 Drive-in Bank
General Urban/Suburban
3.150 KSF

ARF
12/2/2022
1021-22-01537

ITE Study Information

| Peak Hour |
| :--- |
| Weekday |
| AM Peak Street Hour |
| PM Peak Street Hour |
| AM Generator |
| PM Generator |
| Saturday |
| Saturday Generator |
| Sunday |
| Sunday Generator |


| $\#$ | Avg. |
| :---: | :---: |
| Studies | Variable |$|$| 19 | 6 |
| ---: | ---: |
| 44 | 5 |
| 114 | 4 |
| 51 | 5 |
| 57 | 5 |
| 5 | 3 |
| 41 | 4 |
| 5 | 3 |
| 5 | 3 |


| Distribution |  |
| :---: | :---: |
| In | Out |
| $50 \%$ | $50 \%$ |
| $58 \%$ | $42 \%$ |
| $50 \%$ | $50 \%$ |
| $53 \%$ | $47 \%$ |
| $50 \%$ | $50 \%$ |
| $50 \%$ | $50 \%$ |
| $51 \%$ | $49 \%$ |
| $50 \%$ | $50 \%$ |
| $0 \%$ | $0 \%$ |

Trip Generation using ITE Average Rates

| Peak Hour | Rate |  |  |  | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Min. | Avg. | Max. | S.D. | In | Out | Total |
| Weekday | 32.67 | 100.35 | 408.42 | 66.62 | 158 | 158 | 316 |
| AM Peak Street Hour | 2.12 | 9.95 | 29.47 | 6.00 | 18 | 13 | 31 |
| PM Peak Street Hour | 3.04 | 21.01 | 109.91 | 15.13 | 33 | 33 | 66 |
| AM Generator | 4.18 | 14.78 | 47.03 | 9.60 | 25 | 22 | 47 |
| PM Generator | 4.54 | 20.92 | 68.50 | 13.57 | 33 | 33 | 66 |
| Saturday | 42.46 | 86.48 | 171.78 | 38.92 | 136 | 136 | 272 |
| Saturday Generator | 7.18 | 26.35 | 107.00 | 15.32 | 42 | 41 | 83 |
| Sunday | 23.41 | 31.96 | 69.31 | 15.99 | 51 | 50 | 101 |
| Sunday Generator | 3.68 | 4.79 | 7.43 | 1.21 | - | - | 15 |

Trip Generation using ITE Equations

| Peak Hour | Equation | $\mathrm{R}^{2}$ value | Effective Rate | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | In | Out | Total |
| Weekday | Not Given |  | - |  |  | - |
| AM Peak Street Hour | Not Given |  | - |  |  |  |
| PM Peak Street Hour | Not Given |  | - |  |  | - |
| AM Generator | Not Given |  | - |  |  | - |
| PM Generator | Not Given |  | - |  |  | - |
| Saturday | Not Given |  | - |  |  | - |
| Saturday Generator | Not Given |  | - |  |  | - |
| Sunday | Not Given |  | - |  |  | - |
| Sunday Generator | Not Given |  | - |  |  | - |

ITE Land Use Subcategory Description and/or DTraffic Comments:

| Land Use Code: | 912 Drive-in Bank |  |
| :--- | :--- | :--- |
| Setting: | General Urban/Suburban |  |
| Size: | 3.15 | KSF |
| Prepared By: | ARF |  |
| Date: | $12 / 2 / 2022$ |  |
| Job \#: | $1021-22-01537$ |  |

Calculation of Passby Trips

| ip Type | $\begin{gathered} \text { Passby } \\ \% \end{gathered}$ | Trip Generation |  |  | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | In | Out | Total | In | Out |  |


| AM Peak Street Hour |
| :--- |
| Total |
| Passby |
| New (Primary) |


| PM Peak Street Hour |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total | 35\% | $x$ | 33 | 33 | 66 | - | - |  |
| Passby |  |  | 12 | 11 | 23 | - | - | - |
| New (Primary) |  |  | 21 | 22 | 43 | - | - |  |


| AM Generator |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total | 29\% | x | 25 | 22 | 47 | - | - |  |
| Passby |  |  | 7 | 7 | 14 | - | - |  |
| New (Primary) |  |  | 18 | 15 | 33 | - | - |  |


| PM Generator |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total | 35\% | $x$ | 33 | 33 | 66 | - | - |  |
| Passby |  |  | 12 | 11 | 23 | - | - |  |
| New (Primary) |  |  | 21 | 22 | 43 | - | - |  |


| Saturday Generator |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total | 38\% | x | 42 | 41 | 83 | - | - |  |
| Passby |  |  | 16 | 16 | 32 | - | - | - |
| New (Primary) |  |  | 26 | 25 | 51 | - | - |  |

## Passby Comments:

Trip Generation Worksheet, ITE Trip Generation $10^{\text {th }}$ Edition

| Land Use Code: | 150 Warehousing (KSF) |  |
| :--- | :--- | :--- |
| Size: | 927.00 | KSF |
| Prepared By: | ARF |  |
| Date: | $12 / 2 / 2022$ |  |
| Job \#: | $1021-22-01537$ |  |

ITE Study Information

| Peak Hour | \# <br> Studies | Avg. <br> Variable | Distribution |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | In | Out |
| Weekday | 29 | 285 | 50\% | 50\% |
| AM Peak Street Hour | 34 | 451 | 77\% | 23\% |
| PM Peak Street Hour | 47 | 400 | 27\% | 73\% |
| AM Generator | 23 | 274 | 65\% | 35\% |
| PM Generator | 25 | 275 | 24\% | 76\% |
| Saturday | 3 | 226 | 50\% | 50\% |
| Saturday Generator | 2 | 129 | 64\% | 36\% |
| Sunday | 3 | 226 | 50\% | 50\% |
| Sunday Generator | 2 | 129 | 52\% | 48\% |

Trip Generation using ITE Average Rates

| Peak Hour | Rate |  |  |  | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Min. | Avg. | Max. | S.D. | In | Out | Total |
| Weekday | 0.15 | 1.74 | 16.93 | 1.55 | 807 | 806 | 1613 |
| AM Peak Street Hour | 0.02 | 0.17 | 1.93 | 0.20 | 122 | 36 | 158 |
| PM Peak Street Hour | 0.01 | 0.19 | 1.80 | 0.18 | 48 | 128 | 176 |
| AM Generator | 0.02 | 0.22 | 2.08 | 0.28 | 133 | 71 | 204 |
| PM Generator | 0.02 | 0.24 | 1.80 | 0.24 | 53 | 169 | 222 |
| Saturday | 0.01 | 0.15 | 1.58 | 1.12 | 70 | 69 | 139 |
| Saturday Generator | 0.01 | 0.05 | 0.22 |  | 29 | 17 | 46 |
| Sunday | 0.03 | 0.06 | 0.32 | 0.23 | 28 | 28 | 56 |
| Sunday Generator | 0.02 | 0.04 | 0.11 |  | 19 | 18 | 37 |

Trip Generation using ITE Equations

| Peak Hour |
| :--- |
| Weekday |
| AM Peak Street Hour |
| PM Peak Street Hour |
| AM Generator |
| PM Generator |
| Saturday |
| Saturday Generator |
| Sunday |
| Sunday Generator |


| Equation | $\mathrm{R}^{2}$ value | Effective Rate | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | In | Out | Total |
| $\mathrm{T}=1.58(\mathrm{X})+45.54$ | 0.93 | 1.63 | 755 | 755 | 1510 |
| $\mathrm{T}=0.12(\mathrm{X})+25.32$ | 0.69 | 0.15 | 105 | 32 | 137 |
| $\mathrm{T}=0.12(\mathrm{X})+27.82$ | 0.65 | 0.15 | 38 | 101 | 139 |
| $\mathrm{T}=0.11(\mathrm{X})+30.07$ | 0.85 | 0.14 | 86 | 46 | 132 |
| $\mathrm{T}=0.15(\mathrm{X})+22.52$ | 0.91 | 0.17 | 39 | 123 | 162 |
| Not Given |  | - | - | - | - |
| Not Given |  | - | - | - | - |
| Not Given |  | - | - | - | - |
| Not Given |  | - | - | - | - |

DTraffic Comments: Generally accepted as warehouse if < 10\% office use \& if office use is ancillary to warehouse use

| Land Use Code: | 150 Warehousing (KSF) |  |
| :--- | :--- | :--- |
| Size: | 215.20 | KSF |
| Prepared By: | ARF |  |
| Date: | $12 / 2 / 2022$ |  |
| Job \#: | $1021-22-01537$ |  |

ITE Study Information

| Peak Hour |
| :--- |
| Weekday |
| AM Peak Street Hour |
| PM Peak Street Hour |
| AM Generator |
| PM Generator |
| Saturday |
| Saturday Generator |
| Sunday |
| Sunday Generator |


| $\#$ <br> Studies | Avg. <br> Variable |
| ---: | ---: |
| 29 | 285 |
| 34 | 451 |
| 47 | 400 |
| 23 | 274 |
| 25 | 275 |
| 3 | 226 |
| 2 | 129 |
| 3 | 226 |
| 2 | 129 |


| Distribution |  |
| :---: | :---: |
| $\ln$ | Out |
| $50 \%$ | $50 \%$ |
| $77 \%$ | $23 \%$ |
| $27 \%$ | $73 \%$ |
| $65 \%$ | $35 \%$ |
| $24 \%$ | $76 \%$ |
| $50 \%$ | $50 \%$ |
| $64 \%$ | $36 \%$ |
| $50 \%$ | $50 \%$ |
| $52 \%$ | $48 \%$ |

Trip Generation using ITE Average Rates

| Peak Hour | Rate |  |  |  | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Min. | Avg. | Max. | S.D. | In | Out | Total |
| Weekday | 0.15 | 1.74 | 16.93 | 1.55 | 187 | 187 | 374 |
| AM Peak Street Hour | 0.02 | 0.17 | 1.93 | 0.20 | 28 | 9 | 37 |
| PM Peak Street Hour | 0.01 | 0.19 | 1.80 | 0.18 | 11 | 30 | 41 |
| AM Generator | 0.02 | 0.22 | 2.08 | 0.28 | 31 | 16 | 47 |
| PM Generator | 0.02 | 0.24 | 1.80 | 0.24 | 12 | 40 | 52 |
| Saturday | 0.01 | 0.15 | 1.58 | 1.12 | 16 | 16 | 32 |
| Saturday Generator | 0.01 | 0.05 | 0.22 |  | 7 | 4 | 11 |
| Sunday | 0.03 | 0.06 | 0.32 | 0.23 | 7 | 6 | 13 |
| Sunday Generator | 0.02 | 0.04 | 0.11 |  | 5 | 4 | 9 |

Trip Generation using ITE Equations

| Peak Hour |
| :--- |
| Weekday |
| AM Peak Street Hour |
| PM Peak Street Hour |
| AM Generator |
| PM Generator |
| Saturday |
| Saturday Generator |
| Sunday |
| Sunday Generator |


| Equation | $\mathrm{R}^{2}$ value | Effective Rate | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | In | Out | Total |
| $T=1.58(X)+45.54$ | 0.93 | 1.79 | 193 | 193 | 386 |
| $\mathrm{T}=0.12(\mathrm{X})+25.32$ | 0.69 | 0.24 | 39 | 12 | 51 |
| $\mathrm{T}=0.12(\mathrm{X})+27.82$ | 0.65 | 0.25 | 15 | 39 | 54 |
| $\mathrm{T}=0.11(\mathrm{X})+30.07$ | 0.85 | 0.25 | 35 | 19 | 54 |
| $\mathrm{T}=0.15(\mathrm{X})+22.52$ | 0.91 | 0.26 | 13 | 42 | 55 |
| Not Given |  | - | - | - | - |
| Not Given |  | - | - | - | - |
| Not Given |  | - | - | - | - |
| Not Given |  | - | - | - | - |

DTraffic Comments: Generally accepted as warehouse if $<10 \%$ office use \& if office use is ancillary to warehouse use

Trip Generation Worksheet, ITE Trip Generation $11^{\text {th }}$ Edition

Land Use Code:
220 Multifamily Housing (Low-Rise) Not Close to Rail Transit
Setting:
General Urban/Suburban
Size: 246.000 Dwelling Units
Prepared By:
ARF
Date: 12/2/2022
Job \#: 1021-22-01537

ITE Study Information

| Peak Hour |
| :--- |
| Weekday |
| AM Peak Street Hour |
| PM Peak Street Hour |
| AM Generator |
| PM Generator |
| Saturday |
| Saturday Generator |
| Sunday |
| Sunday Generator |


| $\#$ <br> Studies | Avg. <br> Variable |
| ---: | ---: |
| 22 | 229 |
| 49 | 249 |
| 59 | 241 |
| 40 | 234 |
| 38 | 231 |
| 1 | 282 |
| 1 | 282 |
| 1 | 282 |
| 1 | 282 |


| Distribution |  |
| :---: | :---: |
| $\ln$ | Out |
| $50 \%$ | $50 \%$ |
| $24 \%$ | $76 \%$ |
| $63 \%$ | $37 \%$ |
| $24 \%$ | $76 \%$ |
| $62 \%$ | $38 \%$ |
| $50 \%$ | $50 \%$ |
|  |  |
| $50 \%$ | $50 \%$ |
|  |  |

Trip Generation using ITE Average Rates

| Peak Hour | Rate |  |  |  | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Min. | Avg. | Max. | S.D. | In | Out | Total |
| Weekday | 2.46 | 6.74 | 12.50 | 1.79 | 829 | 829 | 1658 |
| AM Peak Street Hour | 0.13 | 0.40 | 0.73 | 0.12 | 24 | 74 | 98 |
| PM Peak Street Hour | 0.08 | 0.51 | 1.04 | 0.15 | 79 | 46 | 125 |
| AM Generator | 0.25 | 0.47 | 0.98 | 0.16 | 28 | 88 | 116 |
| PM Generator | 0.25 | 0.57 | 1.26 | 0.20 | 87 | 53 | 140 |
| Saturday | 4.55 | 4.55 | 4.55 |  | 560 | 559 | 1119 |
| Saturday Generator | 0.41 | 0.41 | 0.41 |  | - | - | 101 |
| Sunday | 3.86 | 3.86 | 3.86 |  | 475 | 475 | 950 |
| Sunday Generator | 0.36 | 0.36 | 0.36 |  | - | - | 89 |

Trip Generation using ITE Equations

| Peak Hour | Equation | $\mathrm{R}^{2}$ value | Effective Rate | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | In | Out | Total |
| Weekday | $\mathrm{T}=6.41(\mathrm{X})+75.31$ | 0.86 | 6.72 | 826 | 826 | 1652 |
| AM Peak Street Hour | $\mathrm{T}=0.31(\mathrm{X})+22.85$ | 0.79 | 0.40 | 24 | 75 | 99 |
| PM Peak Street Hour | T $=0.43(X)+20.55$ | 0.84 | 0.51 | 79 | 47 | 126 |
| AM Generator | $T=0.35(X)+28.13$ | 0.76 | 0.46 | 27 | 87 | 114 |
| PM Generator | $\mathrm{T}=0.42(\mathrm{X})+34.78$ | 0.80 | 0.56 | 86 | 52 | 138 |
| Saturday | Not Given |  | - | - | - | - |
| Saturday Generator | Not Given |  | - | - | - | - |
| Sunday | Not Given |  | - | - | - | - |
| Sunday Generator | Not Given |  | - | - | - | - |

## ITE Land Use Subcategory Description and/or DTraffic Comments:

A site is considered close to rail transit if the walking distance between the residential site entrance and the closest rail transit station is $1 / 2$ mile or less.

It should also be noted that the Resorts World New York City study provides hourly volume data that indicates that the peak hours of traffic for the facility generally occur on Friday and Saturday between 8 PM and 10 PM . Somewhat similar evening peak traffic periods are expected for the proposed Newburgh facility. It is important to note that Newburgh Mall currently closes at 8 PM therefore traffic generation of the remainder of the mall would be minimal during the expected highest peaks of the proposed facility.

## Comparison of Existing Retail Use to Proposed Video Lottery Use

A comparison of the existing traffic generation of the existing $90,000 \mathrm{sq} . \mathrm{ft}$. of retail space to that for the proposed 1,400 VLT entertainment use during peak hours is summarized in Table No. 4 below based on the information contained Tables No. 2 and 3 above.

| TABLE NO. 4 <br> COMPARISON OF TRAFFIC GENERATION VOLUMES EXISTING RETAIL USE VS. PROPOSED VIDEO LOTTERY USE |  |  |  |
| :---: | :---: | :---: | :---: |
| TIME PERIOD | ENTRY | EXIT | TOTAL |
| EXISTING 90,000 SQ. FT. RETAIL SPACE ${ }^{1}$ |  |  |  |
| WEEKDAY PM PEAK | 165 | 179 | 343 |
| SATURDAY AFTERNOON PEAK | 218 | 201 | 419 |
| PROPSOED 1,400 VIDEO LOTTERY TERMINAL FACILITY ${ }^{2}$ |  |  |  |
| WEEKDAY PM PEAK | 189 | 121 | 310 |
| SATURDAY AFTERNOON PEAK | 151 | 163 | 314 |
| SATURDAY EVENING PEAK | 234 | 177 | 411 |
| NOTES: <br> 1. TRAFFIC GENERATION FOR EXISTIN CONTAINED IN TABLE NO. 2. <br> 2. TRAFFIC GENERATION FOR PROPO ESTIMATES AS CONTAINED IN TAB | FT. RETAIL <br> EO LOTTER | 19 TRA <br> BASED | STIMATES AS <br> NYC DATA |

As indicated in the table above, the level of peak hour traffic generation for the proposed VLT use is anticipated to be comparable to the peak hour traffic generation associated with the existing 90,000 sq. ft. of retail space that will be converted for the proposed VLT use. As noted previously, the peak hour of traffic associated with the proposed Resorts World VLT use will occur after the closing of the remainder of the Mall and therefore occur when the other Site related traffic as well as background traffic volumes along the area roadways are significantly lower and thus the anticipated peak traffic of the video lottery facility will be more easily accommodated. Based on the traffic generation comparison between the existing and proposed

```
Land Use Code: 822 Strip Retail Plaza (<40K)
Setting: General Urban/Suburban
Size: 20.000 KSF
Prepared By:
Date:
OSS
11/13/2023
1021 22-01537
```

ITE Study Information

| Peak Hour |  | Avg. Variable | Distribution |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | In | Out |
| Weekday | 4 | 19 | 50\% | 50\% |
| AM Peak Street Hour | 5 | 18 | 60\% | 40\% |
| PM Peak Street Hour | 25 | 21 | 50\% | 50\% |
| AM Generator | 6 | 16 | 50\% | 50\% |
| PM Generator | 5 | 16 | 54\% | 46\% |
| Saturday | 0 | 0 | 0\% | 0\% |
| Saturday Generator | 12 | 27 | 51\% | 49\% |
| Sunday | 0 | 0 | 0\% | 0\% |
| Sunday Generator | 0 | 0 | 0\% | 0\% |

Trip Generation using ITE Average Rates

| Peak Hour | Rate |  |  |  | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Min. | Avg. | Max. | S.D. | In | Out | Total |
| Weekday | 47.86 | 54.45 | 65.07 | 7.81 | 545 | 544 | 1089 |
| AM Peak Street Hour | 1.60 | 2.36 | 3.73 | 0.94 | 28 | 19 | 47 |
| PM Peak Street Hour | 2.81 | 6.59 | 15.20 | 2.94 | 66 | 66 | 132 |
| AM Generator | 2.40 | 7.60 | 21.30 | 6.45 | 76 | 76 | 152 |
| PM Generator | 6.27 | 13.24 | 24.11 | 7.40 | 143 | 122 | 265 |
| Saturday |  |  |  |  | - | - |  |
| Saturday Generator | 1.88 | 6.57 | 14.23 | 3.45 | 67 | 64 | 131 |
| Sunday |  |  |  |  | - | - |  |
| Sunday Generator |  |  |  |  | - | - |  |

Trip Generation using ITE Equations

| Peak Hour |
| :--- |
| Weekday |
| AM Peak Street Hour |
| PM Peak Street Hour |
| AM Generator |
| PM Generator |
| Saturday |
| Saturday Generator |
| Sunday |
| Sunday Generator |


| Equation | $\mathrm{R}^{2}$ value | Effective Rate | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | In | Out | Total |
| $\mathrm{T}=42.20(\mathrm{X})+229.68$ | 0.96 | 53.70 | 537 | 537 | 1074 |
| $\operatorname{Ln}(\mathrm{T})=0.66 \operatorname{Ln}(\mathrm{X})+1.84$ | 0.57 | 2.25 | 27 | 18 | 45 |
| $\operatorname{Ln}(\mathrm{T})=0.71 \operatorname{Ln}(\mathrm{X})+2.72$ | 0.56 | 6.35 | 64 | 63 | 127 |
| Not Given | 0.00 | 0.05 | 1 | 0 | 1 |
| Not Given | 0.00 | 0.05 | 1 | 0 | 1 |
| Not Given | 0.00 | 0.05 | - | - | 1 |
| Not Given | 0.00 | 0.05 | 1 | 0 | 1 |
| Not Given | 0.00 | 0.05 | - | - | 1 |
| Not Given |  | - | - | - | - |

ITE Land Use Subcategory Description and/or DTraffic Comments:

```
Land Use Code: }150\mathrm{ Warehousing
Setting: General Urban/Suburban
Size: 173.000 KSF
Prepared By:
OSS
11/13/2023
1021 22-01537
```

ITE Study Information

| Peak Hour | $\begin{gathered} \# \\ \text { Studies } \end{gathered}$ | Avg. Variable | Distribution |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | In | Out |
| Weekday | 31 | 292 | 50\% | 50\% |
| AM Peak Street Hour | 36 | 448 | 77\% | 23\% |
| PM Peak Street Hour | 49 | 400 | 28\% | 72\% |
| AM Generator | 25 | 284 | 66\% | 34\% |
| PM Generator | 27 | 284 | 24\% | 76\% |
| Saturday | 3 | 226 | 50\% | 50\% |
| Saturday Generator | 2 | 129 | 64\% | 36\% |
| Sunday | 3 | 226 | 50\% | 50\% |
| Sunday Generator | 2 | 129 | 52\% | 48\% |

Trip Generation using ITE Average Rates

| Peak Hour | Rate |  |  |  | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Min. | Avg. | Max. | S.D. | In | Out | Total |
| Weekday | 0.15 | 1.71 | 16.93 | 1.48 | 148 | 148 | 296 |
| AM Peak Street Hour | 0.02 | 0.17 | 1.93 | 0.19 | 22 | 7 | 29 |
| PM Peak Street Hour | 0.01 | 0.18 | 1.80 | 0.18 | 9 | 22 | 31 |
| AM Generator | 0.02 | 0.21 | 2.06 | 0.26 | 24 | 12 | 36 |
| PM Generator | 0.02 | 0.23 | 1.80 | 0.23 | 10 | 30 | 40 |
| Saturday | 0.01 | 0.15 | 1.58 | 0.53 | 13 | 13 | 26 |
| Saturday Generator | 0.01 | 0.05 | 0.22 |  | 6 | 3 | 9 |
| Sunday | 0.03 | 0.06 | 0.32 | 0.10 | 5 | 5 | 10 |
| Sunday Generator | 0.02 | 0.04 | 0.11 |  | 4 | 3 | 7 |

Trip Generation using ITE Equations

| Peak Hour | Equation | $\mathrm{R}^{2}$ value | Effective Rate | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | In | Out | Total |
| Weekday | $\mathrm{T}=1.58(\mathrm{X})+38.29$ | 0.92 | 1.80 | 156 | 156 | 312 |
| AM Peak Street Hour | $\mathrm{T}=0.12(\mathrm{X})+23.62$ | 0.69 | 0.25 | 34 | 10 | 44 |
| PM Peak Street Hour | $\mathrm{T}=0.12(\mathrm{X})+26.48$ | 0.65 | 0.27 | 13 | 34 | 47 |
| AM Generator | $\mathrm{T}=0.11(\mathrm{X})+28.55$ | 0.85 | 0.28 | 32 | 16 | 48 |
| PM Generator | $\mathrm{T}=0.15(\mathrm{X})+20.47$ | 0.90 | 0.27 | 11 | 35 | 46 |
| Saturday | Not Given |  | - | - | - | - |
| Saturday Generator | Not Given |  | - |  | - | - |
| Sunday | Not Given |  | - | - | - | - |
| Sunday Generator | Not Given |  | - | - | - | - |

ITE Land Use Subcategory Description and/or DTraffic Comments:

```
Land Use Code: }150\mathrm{ Warehousing
Setting: General Urban/Suburban
Size: 56.000 KSF
Prepared By:
Date:
OSS
11/13/2023
1021 22-01537
```

ITE Study Information

| Peak Hour | $\begin{gathered} \# \\ \text { Studies } \end{gathered}$ | Avg. Variable | Distribution |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | In | Out |
| Weekday | 31 | 292 | 50\% | 50\% |
| AM Peak Street Hour | 36 | 448 | 77\% | 23\% |
| PM Peak Street Hour | 49 | 400 | 28\% | 72\% |
| AM Generator | 25 | 284 | 66\% | 34\% |
| PM Generator | 27 | 284 | 24\% | 76\% |
| Saturday | 3 | 226 | 50\% | 50\% |
| Saturday Generator | 2 | 129 | 64\% | 36\% |
| Sunday | 3 | 226 | 50\% | 50\% |
| Sunday Generator | 2 | 129 | 52\% | 48\% |

Trip Generation using ITE Average Rates

| Peak Hour | Rate |  |  |  | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Min. | Avg. | Max. | S.D. | In | Out | Total |
| Weekday | 0.15 | 1.71 | 16.93 | 1.48 | 48 | 48 | 96 |
| AM Peak Street Hour | 0.02 | 0.17 | 1.93 | 0.19 | 8 | 2 | 10 |
| PM Peak Street Hour | 0.01 | 0.18 | 1.80 | 0.18 | 3 | 7 | 10 |
| AM Generator | 0.02 | 0.21 | 2.06 | 0.26 | 8 | 4 | 12 |
| PM Generator | 0.02 | 0.23 | 1.80 | 0.23 | 3 | 10 | 13 |
| Saturday | 0.01 | 0.15 | 1.58 | 0.53 | 4 | 4 | 8 |
| Saturday Generator | 0.01 | 0.05 | 0.22 |  | 2 | 1 | 3 |
| Sunday | 0.03 | 0.06 | 0.32 | 0.10 | 2 | 1 | 3 |
| Sunday Generator | 0.02 | 0.04 | 0.11 |  | 1 | 1 | 2 |

Trip Generation using ITE Equations

| Peak Hour | Equation | $\mathrm{R}^{2}$ value | Effective Rate | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | In | Out | Total |
| Weekday | $\mathrm{T}=1.58(\mathrm{X})+38.29$ | 0.92 | 2.27 | 64 | 63 | 127 |
| AM Peak Street Hour | $\mathrm{T}=0.12(\mathrm{X})+23.62$ | 0.69 | 0.54 | 23 | 7 | 30 |
| PM Peak Street Hour | $\mathrm{T}=0.12(\mathrm{X})+26.48$ | 0.65 | 0.59 | 9 | 24 | 33 |
| AM Generator | $\mathrm{T}=0.11(\mathrm{X})+28.55$ | 0.85 | 0.63 | 23 | 12 | 35 |
| PM Generator | $\mathrm{T}=0.15(\mathrm{X})+20.47$ | 0.90 | 0.52 | 7 | 22 | 29 |
| Saturday | Not Given |  |  | - | - | - |
| Saturday Generator | Not Given |  |  | - | - | - |
| Sunday | Not Given |  | - | - | - | - |
| Sunday Generator | Not Given |  | - | - | - | - |

ITE Land Use Subcategory Description and/or DTraffic Comments:

Trip Generation Worksheet, ITE Trip Generation $11^{\text {th }}$ Edition

```
Land Use Code: }720\mathrm{ Medical-Dental Office Building - Stand Alone
Setting: General Urban/Suburban
Size: 3.515 KSF
Prepared By:
Date:
OSS
1/16/2024
1021 22-01537
```

ITE Study Information

| Peak Hour |
| :--- |
| Weekday |
| AM Peak Street Hour |
| PM Peak Street Hour |
| AM Generator |
| PM Generator |
| Saturday |
| Saturday Generator |
| Sunday |
| Sunday Generator |


| \# <br> Studies | Avg. |
| ---: | ---: |
| Variable |  |$|$| 18 | 15 |
| ---: | ---: |
| 24 | 25 |
| 30 | 23 |
| 21 | 15 |
| 22 | 18 |
| 3 | 31 |
| 2 | 34 |
| 2 | 34 |
| 2 | 34 |


| Distribution |  |
| :---: | :---: |
| In | Out |
| $50 \%$ | $50 \%$ |
| $79 \%$ | $21 \%$ |
| $30 \%$ | $70 \%$ |
| $59 \%$ | $41 \%$ |
| $40 \%$ | $60 \%$ |
| $50 \%$ | $50 \%$ |
| $57 \%$ | $43 \%$ |
| $50 \%$ | $50 \%$ |
| $52 \%$ | $48 \%$ |

Trip Generation using ITE Average Rates

| Peak Hour | Rate |  |  |  | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Min. | Avg. | Max. | S.D. | In | Out | Total |
| Weekday | 14.52 | 36.00 | 100.75 | 13.38 | 64 | 63 | 127 |
| AM Peak Street Hour | 0.87 | 3.10 | 14.30 | 1.49 | 9 | 2 | 11 |
| PM Peak Street Hour | 0.62 | 3.93 | 8.86 | 1.86 | 4 | 10 | 14 |
| AM Generator | 1.21 | 3.74 | 19.28 | 2.14 | 8 | 5 | 13 |
| PM Generator | 1.88 | 4.79 | 15.55 | 1.62 | 7 | 10 | 17 |
| Saturday | 5.24 | 13.78 | 21.93 | 9.26 | 24 | 24 | 48 |
| Saturday Generator | 1.33 | 3.02 | 4.02 |  | 6 | 5 | 11 |
| Sunday | 0.39 | 1.14 | 1.58 |  | 2 | 2 | 4 |
| Sunday Generator | 0.12 | 0.22 | 0.28 |  | 1 | 0 | 1 |

Trip Generation using ITE Equations

| Peak Hour | Equation | $\mathrm{R}^{2}$ value | Effective Rate | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | In | Out | Total |
| Weekday | $\mathrm{T}=42.97(\mathrm{X})-108.01$ | 0.92 | 12.23 | 22 | 21 | 43 |
| AM Peak Street Hour | $\operatorname{Ln}(\mathrm{T})=0.90 \operatorname{Ln}(\mathrm{X})+1.34$ | 0.80 | 3.41 | 9 | 3 | 12 |
| PM Peak Street Hour | $\mathrm{T}=4.07(\mathrm{X})-3.17$ | 0.77 | 3.13 | 3 | 8 | 11 |
| AM Generator | T $=3.56(X)+2.66$ | 0.74 | 4.27 | 9 | 6 | 15 |
| PM Generator | T = 5.36(X) - 10.42 | 0.95 | 2.28 | 3 | 5 | 8 |
| Saturday | Not Given |  | - | - | - | - |
| Saturday Generator | Not Given |  | - | - | - | - |
| Sunday | Not Given |  | - | - | - | - |
| Sunday Generator | Not Given |  | - | - | - | - |

## ITE Land Use Subcategory Description and/or DTraffic Comments:

Per ITE, "Analysis of medical-dental office building data found that trip generation rates are measurably different for sites located within or adjacent to a hospital campus and sites that are stand-alone."

Land Use Code:
Setting:
Size:
Prepared By:
Date:
Job \#:

151 Mini-Warehouse
General Urban/Suburban
85.000 KSF

OSS
1/16/2024
1021 22-01537

ITE Study Information

| Peak Hour |
| :--- |
| Weekday |
| AM Peak Street Hour |
| PM Peak Street Hour |
| AM Generator |
| PM Generator |
| Saturday |
| Saturday Generator |
| Sunday |
| Sunday Generator |


| $\#$ | Avg. |
| ---: | ---: |
| Studies | Variable |$|$| 16 | 55 |
| ---: | ---: |
| 13 | 70 |
| 18 | 59 |
| 11 | 66 |
| 16 | 56 |
| 6 | 43 |
| 3 | 90 |
| 5 | 40 |
| 2 | 79 |


| Distribution |  |
| :---: | :---: |
| In | Out |
| $50 \%$ | $50 \%$ |
| $59 \%$ | $41 \%$ |
| $47 \%$ | $53 \%$ |
| $51 \%$ | $49 \%$ |
| $51 \%$ | $49 \%$ |
| $50 \%$ | $50 \%$ |
| $62 \%$ | $38 \%$ |
| $50 \%$ | $50 \%$ |
| $45 \%$ | $55 \%$ |

Trip Generation using ITE Average Rates

| Peak Hour | Rate |  |  |  | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Min. | Avg. | Max. | S.D. | In | Out | Total |
| Weekday | 0.38 | 1.45 | 3.25 | 0.92 | 62 | 61 | 123 |
| AM Peak Street Hour | 0.04 | 0.09 | 0.17 | 0.05 | 5 | 3 | 8 |
| PM Peak Street Hour | 0.02 | 0.15 | 0.64 | 0.14 | 6 | 7 | 13 |
| AM Generator | 0.07 | 0.18 | 0.79 | 0.16 | 8 | 7 | 15 |
| PM Generator | 0.06 | 0.18 | 1.05 | 0.14 | 8 | 7 | 15 |
| Saturday | 1.21 | 1.77 | 3.29 | 0.76 | 75 | 75 | 150 |
| Saturday Generator | 0.04 | 0.17 | 0.31 | 0.14 | 9 | 5 | 14 |
| Sunday | 0.69 | 1.50 | 3.70 | 1.01 | 64 | 64 | 128 |
| Sunday Generator | 0.16 | 0.20 | 0.23 |  | 8 | 9 | 17 |

Trip Generation using ITE Equations

| Peak Hour | Equation | $\mathrm{R}^{2}$ value | Effective Rate | Trip Generation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | In | Out | Total |
| Weekday | Not Given |  | - | - |  | - |
| AM Peak Street Hour | Not Given |  | - | - | - | - |
| PM Peak Street Hour | Not Given |  | - | - | - | - |
| AM Generator | Not Given |  | - | - |  | - |
| PM Generator | Not Given |  | - | - | - | - |
| Saturday | $\mathrm{T}=1.00(\mathrm{X})+33.19$ | 0.57 | 1.39 | 59 | 59 | 118 |
| Saturday Generator | Not Given |  | - | - |  | - |
| Sunday | Not Given |  | - | - | - | - |
| Sunday Generator | Not Given |  | - | - | - | - |

ITE Land Use Subcategory Description and/or DTraffic Comments:

## Appendix C <br> Capacity Analysis

|  | 4 | $\rightarrow$ | 7 | 7 | $4$ |  | $4$ | $\dagger$ |  | , | $\frac{1}{1}$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 |  |  | $\uparrow$ | F' | * | $\uparrow$ |  | ${ }^{*}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 69 | 259 | 166 | 44 | 341 | 90 | 254 | 581 | 45 | 79 | 418 | 70 |
| Future Volume (vph) | 69 | 259 | 166 | 44 | 341 | 90 | 254 | 581 | 45 | 79 | 418 | 70 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 11 | 11 | 11 | 11 | 14 | 14 | 11 | 11 | 11 |
| Grade (\%) |  | -2\% |  |  | 1\% |  |  | -4\% |  |  | -1\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 140 | 256 |  | 0 | 260 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.955 |  |  |  | 0.850 |  | 0.989 |  |  | 0.978 |  |
| Flt Protected |  | 0.993 |  |  | 0.994 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1774 | 0 | 0 | 1797 | 1538 | 1762 | 2023 | 0 | 1702 | 1772 | 0 |
| Flt Permitted |  | 0.741 |  |  | 0.891 |  | 0.204 |  |  | 0.145 |  |  |
| Satd. Flow (perm) | 0 | 1324 | 0 | 0 | 1610 | 1538 | 378 | 2023 | 0 | 260 | 1772 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 23 |  |  |  | 70 |  | 5 |  |  | 10 |  |
| Link Speed (mph) |  | 40 |  |  | 40 |  |  | 40 |  |  | 40 |  |
| Link Distance (ft) |  | 155 |  |  | 698 |  |  | 257 |  |  | 538 |  |
| Travel Time (s) |  | 2.6 |  |  | 11.9 |  |  | 4.4 |  |  | 9.2 |  |
| Peak Hour Factor | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 |
| Heavy Vehicles (\%) | 1\% | 4\% | 1\% | 2\% | 1\% | 1\% | 1\% | 1\% | 2\% | 3\% | 2\% | 1\% |
| Adj. Flow (vph) | 70 | 262 | 168 | 44 | 344 | 91 | 257 | 587 | 45 | 80 | 422 | 71 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 500 | 0 | 0 | 388 | 91 | 257 | 632 | 0 | 80 | 493 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 | 8 | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Minimum Split (s) | 8.0 | 8.0 |  | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 |  | 8.0 | 8.0 |  |
| Total Split (s) | 40.0 | 40.0 |  | 40.0 | 40.0 | 40.0 | 15.0 | 60.0 |  | 15.0 | 60.0 |  |
| Total Split (\%) | 34.8\% | 34.8\% |  | 34.8\% | 34.8\% | 34.8\% | 13.0\% | 52.2\% |  | 13.0\% | 52.2\% |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 5.0 |  |  | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  | Lead | Lag |  | Lead | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes | Yes |  |
| Recall Mode | None | None |  | None | None | None | None | Min |  | None | Min |  |
| Act Effct Green (s) |  | 35.4 |  |  | 35.4 | 35.4 | 45.0 | 37.2 |  | 40.2 | 32.4 |  |
| Actuated g/C Ratio |  | 0.38 |  |  | 0.38 | 0.38 | 0.48 | 0.40 |  | 0.43 | 0.35 |  |
| v/c Ratio |  | 0.96 |  |  | 0.63 | 0.14 | 0.77 | 0.77 |  | 0.34 | 0.79 |  |
| Control Delay (s/veh) |  | 62.5 |  |  | 31.7 | 9.3 | 30.5 | 32.3 |  | 15.2 | 36.1 |  |
| Queue Delay |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay (s/veh) |  | 62.5 |  |  | 31.7 | 9.3 | 30.5 | 32.3 |  | 15.2 | 36.1 |  |
| LOS |  | E |  |  | C | A | C | C |  | B | D |  |
| Approach Delay (s/veh) |  | 62.5 |  |  | 27.5 |  |  | 31.8 |  |  | 33.2 |  |

AMC
Synchro 11 Report
Lanes, Volumes, Timings


Splits and Phases: $\quad$ 10: Union Avenue (NYS Route 300) \& South Plank Road (NYS Route 52)


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \$ |  |  | $\uparrow$ | F' | ${ }^{7}$ | 个 |  | \% | $\hat{1}$ |  |
| Traffic Volume (veh/h) | 69 | 259 | 166 | 44 | 341 | 90 | 254 | 581 | 45 | 79 | 418 | 70 |
| Future Volume (veh/h) | 69 | 259 | 166 | 44 | 341 | 90 | 254 | 581 | 45 | 79 | 418 | 70 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1964 | 1919 | 1964 | 1864 | 1879 | 1879 | 2042 | 2124 | 2108 | 1894 | 1909 | 1924 |
| Adj Flow Rate, veh/h | 70 | 262 | 168 | 44 | 344 | 91 | 257 | 587 | 45 | 80 | 422 | 71 |
| Peak Hour Factor | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 |
| Percent Heavy Veh, \% | 1 | 4 | 1 | 2 | 1 | 1 | 1 | 1 | 2 | 3 | 2 | 1 |
| Cap, veh/h | 101 | 311 | 183 | 92 | 594 | 625 | 367 | 732 | 56 | 259 | 497 | 84 |
| Arrive On Green | 0.39 | 0.39 | 0.39 | 0.39 | 0.39 | 0.39 | 0.11 | 0.38 | 0.38 | 0.05 | 0.31 | 0.31 |
| Sat Flow, veh/h | 130 | 792 | 466 | 109 | 1514 | 1593 | 1945 | 1948 | 149 | 1804 | 1593 | 268 |
| Grp Volume(v), veh/h | 500 | 0 | 0 | 388 | 0 | 91 | 257 | 0 | 632 | 80 | 0 | 493 |
| Grp Sat Flow(s),veh/h/ln | 1388 | 0 | 0 | 1622 | 0 | 1593 | 1945 | 0 | 2097 | 1804 | 0 | 1861 |
| Q Serve(g_s), s | 15.1 | 0.0 | 0.0 | 0.0 | 0.0 | 3.0 | 6.8 | 0.0 | 21.8 | 2.4 | 0.0 | 20.1 |
| Cycle Q Clear(g_c), s | 28.6 | 0.0 | 0.0 | 13.5 | 0.0 | 3.0 | 6.8 | 0.0 | 21.8 | 2.4 | 0.0 | 20.1 |
| Prop In Lane | 0.14 |  | 0.34 | 0.11 |  | 1.00 | 1.00 |  | 0.07 | 1.00 |  | 0.14 |
| Lane Grp Cap(c), veh/h | 595 | 0 | 0 | 686 | 0 | 625 | 367 | 0 | 788 | 259 | 0 | 581 |
| V/C Ratio(X) | 0.84 | 0.00 | 0.00 | 0.57 | 0.00 | 0.15 | 0.70 | 0.00 | 0.80 | 0.31 | 0.00 | 0.85 |
| Avail Cap(c_a), veh/h | 658 | 0 | 0 | 752 | 0 | 687 | 392 | 0 | 1421 | 397 | 0 | 1261 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(1) | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 24.0 | 0.0 | 0.0 | 18.9 | 0.0 | 15.9 | 18.2 | 0.0 | 22.6 | 19.4 | 0.0 | 26.1 |
| Incr Delay (d2), s/veh | 8.8 | 0.0 | 0.0 | 0.8 | 0.0 | 0.1 | 5.1 | 0.0 | 2.0 | 0.7 | 0.0 | 3.6 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 9.8 | 0.0 | 0.0 | 5.2 | 0.0 | 1.0 | 3.2 | 0.0 | 10.1 | 1.0 | 0.0 | 8.7 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d), s/veh | 32.8 | 0.0 | 0.0 | 19.7 | 0.0 | 16.0 | 23.3 | 0.0 | 24.6 | 20.0 | 0.0 | 29.7 |
| LnGrp LOS | C |  |  | B |  | B | C |  | C | C |  | C |
| Approach Vol, veh/h |  | 500 |  |  | 479 |  |  | 889 |  |  | 573 |  |
| Approach Delay, s/veh |  | 32.8 |  |  | 19.0 |  |  | 24.2 |  |  | 28.3 |  |
| Approach LOS |  | C |  |  | B |  |  | C |  |  | C |  |


| Timer - Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$, s | 8.8 | 35.5 | 36.9 | 14.0 | 30.3 | 36.9 |
| Change Period (Y+Rc), s | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Max Green Setting (Gmax), s | 10.0 | 55.0 | 35.0 | 10.0 | 55.0 | 35.0 |
| Max Q Clear Time (g_c+11), s | 4.4 | 23.8 | 30.6 | 8.8 | 22.1 | 15.5 |
| Green Ext Time (p_c), s | 0.1 | 4.4 | 1.3 | 0.2 | 3.2 | 2.7 |

Intersection Summary
HCM 6th Ctrl Delay, s/veh 25.9
HCM 6th LOS
C

|  | $\rangle$ |  |  |  |  |  | 4 | $\uparrow$ |  |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\dagger$ |  |  | $\uparrow$ | F | ${ }^{*}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 73 | 201 | 186 | 47 | 173 | 86 | 213 | 553 | 37 | 71 | 522 | 61 |
| Future Volume (vph) | 73 | 201 | 186 | 47 | 173 | 86 | 213 | 553 | 37 | 71 | 522 | 61 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 11 | 11 | 11 | 11 | 14 | 14 | 11 | 11 | 11 |
| Grade (\%) |  | -2\% |  |  | 1\% |  |  | -4\% |  |  | -1\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 140 | 256 |  | 0 | 260 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.945 |  |  |  | 0.850 |  | 0.991 |  |  | 0.984 |  |
| Flt Protected |  | 0.992 |  |  | 0.989 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1777 | 0 | 0 | 1793 | 1553 | 1762 | 2030 | 0 | 1754 | 1795 | 0 |
| Flt Permitted |  | 0.903 |  |  | 0.800 |  | 0.140 |  |  | 0.213 |  |  |
| Satd. Flow (perm) | 0 | 1617 | 0 | 0 | 1451 | 1553 | 260 | 2030 | 0 | 393 | 1795 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 31 |  |  |  | 89 |  | 4 |  |  | 7 |  |
| Link Speed (mph) |  | 40 |  |  | 40 |  |  | 40 |  |  | 40 |  |
| Link Distance (ft) |  | 155 |  |  | 698 |  |  | 257 |  |  | 538 |  |
| Travel Time (s) |  | 2.6 |  |  | 11.9 |  |  | 4.4 |  |  | 9.2 |  |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Heavy Vehicles (\%) | 0\% | 1\% | 2\% | 0\% | 1\% | 0\% | 1\% | 1\% | 0\% | 0\% | 1\% | 3\% |
| Adj. Flow (vph) | 75 | 207 | 192 | 48 | 178 | 89 | 220 | 570 | 38 | 73 | 538 | 63 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 474 | 0 | 0 | 226 | 89 | 220 | 608 | 0 | 73 | 601 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | , |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 | 8 | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Minimum Split (s) | 8.0 | 8.0 |  | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 |  | 8.0 | 8.0 |  |
| Total Split (s) | 40.0 | 40.0 |  | 40.0 | 40.0 | 40.0 | 15.0 | 60.0 |  | 15.0 | 60.0 |  |
| Total Split (\%) | 34.8\% | 34.8\% |  | 34.8\% | 34.8\% | 34.8\% | 13.0\% | 52.2\% |  | 13.0\% | 52.2\% |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 5.0 |  |  | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  | Lead | Lag |  | Lead | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes | Yes |  |
| Recall Mode | None | None |  | None | None | None | None | Min |  | None | Min |  |
| Act Effct Green (s) |  | 35.4 |  |  | 35.4 | 35.4 | 50.8 | 43.0 |  | 45.6 | 38.0 |  |
| Actuated g/C Ratio |  | 0.36 |  |  | 0.36 | 0.36 | 0.52 | 0.44 |  | 0.46 | 0.39 |  |
| v/c Ratio |  | 0.79 |  |  | 0.43 | 0.14 | 0.76 | 0.68 |  | 0.25 | 0.86 |  |
| Control Delay (s/veh) |  | 39.6 |  |  | 29.8 | 6.6 | 33.9 | 27.2 |  | 12.6 | 40.7 |  |
| Queue Delay |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay (s/veh) |  | 39.6 |  |  | 29.8 | 6.6 | 33.9 | 27.2 |  | 12.6 | 40.7 |  |
| LOS |  | D |  |  | C | A | C | C |  | B | D |  |
| Approach Delay (s/veh) |  | 39.7 |  |  | 23.3 |  |  | 29.1 |  |  | 37.7 |  |

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Splits and Phases: $\quad$ 10: Union Avenue (NYS Route 300) \& South Plank Road (NYS Route 52)



| LnGrp Delay(d), s/veh | 27.3 | 0.0 | 0.0 | 19.6 | 0.0 | 17.9 | 17.9 | 0.0 | 18.2 | 15.0 | 0.0 | 24.6 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LnGrp LOS | C |  |  | B |  | B | B |  | B | B |  | C |
| Approach Vol, veh/h |  | 474 |  |  | 315 |  |  | 828 |  |  | 674 |  |
| Approach Delay, s/veh |  | 27.3 |  |  | 19.1 |  |  | 18.1 |  |  | 23.6 |  |
| Approach LOS |  | C |  |  | B |  |  | B |  |  | C |  |


| Timer - Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration (G+Y+Rc), s | 8.1 | 37.2 | 29.9 | 12.2 | 33.1 | 29.9 |
| Change Period (Y+Rc), s | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Max Green Setting (Gmax), s | 10.0 | 55.0 | 35.0 | 10.0 | 55.0 | 35.0 |
| Max Q Clear Time (g_c+11), s | 3.8 | 19.5 | 22.5 | 6.9 | 24.0 | 8.9 |
| Green Ext Time (p_c), s | 0.1 | 4.2 | 2.4 | 0.3 | 4.1 | 1.9 |

## Intersection Summary

HCM 6th Ctrl Delay, s/veh 21.8
HCM 6th LOS
C

|  | 4 | $\rightarrow$ | 7 | 7 | $4$ |  | $4$ | $\dagger$ |  | , | $\frac{1}{1}$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 |  |  | $\uparrow$ | 「 | ${ }^{*}$ | $\hat{\beta}$ |  | \% | $\uparrow$ |  |
| Traffic Volume (vph) | 86 | 286 | 212 | 46 | 372 | 122 | 290 | 779 | 47 | 106 | 578 | 87 |
| Future Volume (vph) | 86 | 286 | 212 | 46 | 372 | 122 | 290 | 779 | 47 | 106 | 578 | 87 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 11 | 11 | 11 | 11 | 14 | 14 | 11 | 11 | 11 |
| Grade (\%) |  | -2\% |  |  | 1\% |  |  | -4\% |  |  | -1\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 140 | 256 |  | 0 | 260 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.951 |  |  |  | 0.850 |  | 0.992 |  |  | 0.980 |  |
| Flt Protected |  | 0.993 |  |  | 0.995 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1769 | 0 | 0 | 1798 | 1538 | 1762 | 2029 | 0 | 1702 | 1776 | 0 |
| Flt Permitted |  | 0.517 |  |  | 0.817 |  | 0.130 |  |  | 0.087 |  |  |
| Satd. Flow (perm) | 0 | 921 | 0 | 0 | 1477 | 1538 | 241 | 2029 | 0 | 156 | 1776 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 26 |  |  |  | 87 |  | 4 |  |  | 9 |  |
| Link Speed (mph) |  | 40 |  |  | 40 |  |  | 40 |  |  | 40 |  |
| Link Distance (ft) |  | 155 |  |  | 698 |  |  | 257 |  |  | 538 |  |
| Travel Time (s) |  | 2.6 |  |  | 11.9 |  |  | 4.4 |  |  | 9.2 |  |
| Peak Hour Factor | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 |
| Heavy Vehicles (\%) | 1\% | 4\% | 1\% | 2\% | 1\% | 1\% | 1\% | 1\% | 2\% | 3\% | 2\% | 1\% |
| Adj. Flow (vph) | 87 | 289 | 214 | 46 | 376 | 123 | 293 | 787 | 47 | 107 | 584 | 88 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 590 | 0 | 0 | 422 | 123 | 293 | 834 | 0 | 107 | 672 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 | 8 | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Minimum Split (s) | 8.0 | 8.0 |  | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 |  | 8.0 | 8.0 |  |
| Total Split (s) | 40.0 | 40.0 |  | 40.0 | 40.0 | 40.0 | 15.0 | 60.0 |  | 15.0 | 60.0 |  |
| Total Split (\%) | 34.8\% | 34.8\% |  | 34.8\% | 34.8\% | 34.8\% | 13.0\% | 52.2\% |  | 13.0\% | 52.2\% |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 5.0 |  |  | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  | Lead | Lag |  | Lead | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes | Yes |  |
| Recall Mode | None | None |  | None | None | None | None | Min |  | None | Min |  |
| Act Effct Green (s) |  | 35.3 |  |  | 35.3 | 35.3 | 57.8 | 47.7 |  | 54.8 | 46.2 |  |
| Actuated g/C Ratio |  | 0.33 |  |  | 0.33 | 0.33 | 0.54 | 0.45 |  | 0.51 | 0.43 |  |
| v/c Ratio |  | 1.83 |  |  | 0.86 | 0.21 | 1.06 | 0.91 |  | 0.52 | 0.86 |  |
| Control Delay (s/veh) |  | 412.4 |  |  | 54.5 | 11.6 | 96.7 | 43.2 |  | 23.1 | 39.6 |  |
| Queue Delay |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay (s/veh) |  | 412.4 |  |  | 54.5 | 11.6 | 96.7 | 43.2 |  | 23.1 | 39.6 |  |
| LOS |  | F |  |  | D | B | F | D |  | C | D |  |
| Approach Delay (s/veh) |  | 412.4 |  |  | 44.9 |  |  | 57.2 |  |  | 37.4 |  |

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|  |  |  |  |  |  | 4 | 4 |  |  | $\dagger$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Approach LOS | F |  |  | D |  |  | E |  |  | D |  |
| Queue Length 50th (ft) | $\sim 638$ |  |  | 285 | 18 | ~146 | 516 |  | 31 | 400 |  |
| Queue Length 95th (ft) | \#898 |  |  | \#502 | 65 | \#331 | \#776 |  | 73 | 564 |  |
| Internal Link Dist (ft) | 75 |  |  | 618 |  |  | 177 |  |  | 458 |  |
| Turn Bay Length (ft) |  |  |  |  | 140 | 256 |  |  | 260 |  |  |
| Base Capacity (vph) | 321 |  |  | 488 | 566 | 274 | 1056 |  | 228 | 927 |  |
| Starvation Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 1.84 |  |  | 0.86 | 0.22 | 1.07 | 0.79 |  | 0.47 | 0.72 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 115 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 106.7 |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.84 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay (s/veh): 118.8 |  |  |  | Intersection LOS: F |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 123.3\% |  |  |  | ICU Level of Service H |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 10: Union Avenue (NYS Route 300) \& South Plank Road (NYS Route 52)


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \＄ |  |  | $\uparrow$ | 「 | ${ }^{*}$ | 个 |  | ${ }^{7}$ | 今 |  |
| Traffic Volume（veh／h） | 86 | 286 | 212 | 46 | 372 | 122 | 290 | 779 | 47 | 106 | 578 | 87 |
| Future Volume（veh／h） | 86 | 286 | 212 | 46 | 372 | 122 | 290 | 779 | 47 | 106 | 578 | 87 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1964 | 1919 | 1964 | 1864 | 1879 | 1879 | 2042 | 2124 | 2108 | 1894 | 1909 | 1924 |
| Adj Flow Rate，veh／h | 87 | 289 | 214 | 46 | 376 | 123 | 293 | 787 | 47 | 107 | 584 | 88 |
| Peak Hour Factor | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 |
| Percent Heavy Veh，\％ |  | 4 | 1 | 2 | 1 | 1 | 1 | 1 | 2 | 3 | 2 | 1 |
| Cap，veh／h | 68 | 154 | 103 | 77 | 492 | 557 | 319 | 887 | 53 | 224 | 649 | 98 |
| Arrive On Green | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | 0.10 | 0.45 | 0.45 | 0.05 | 0.40 | 0.40 |
| Sat Flow，veh／h | 75 | 440 | 293 | 105 | 1406 | 1593 | 1945 | 1984 | 118 | 1804 | 1621 | 244 |
| Grp Volume（v），veh／h | 590 | 0 | 0 | 422 | 0 | 123 | 293 | 0 | 834 | 107 | 0 | 672 |
| Grp Sat Flow（s），veh／h／n | 808 | 0 | 0 | 1510 | 0 | 1593 | 1945 | 0 | 2103 | 1804 | 0 | 1865 |
| Q Serve（g＿s），s | 11.4 | 0.0 | 0.0 | 0.0 | 0.0 | 5.4 | 8.6 | 0.0 | 36.4 | 3.4 | 0.0 | 33.8 |
| Cycle Q Clear（g＿c），s | 35.0 | 0.0 | 0.0 | 23.6 | 0.0 | 5.4 | 8.6 | 0.0 | 36.4 | 3.4 | 0.0 | 33.8 |
| Prop In Lane | 0.15 |  | 0.36 | 0.11 |  | 1.00 | 1.00 |  | 0.06 | 1.00 |  | 0.13 |
| Lane Grp Cap（c），veh／h | 324 | 0 | 0 | 568 | 0 | 557 | 319 | 0 | 940 | 224 | 0 | 747 |
| V／C Ratio（X） | 1.82 | 0.00 | 0.00 | 0.74 | 0.00 | 0.22 | 0.92 | 0.00 | 0.89 | 0.48 | 0.00 | 0.90 |
| Avail Cap（c＿a），veh／h | 324 | 0 | 0 | 568 | 0 | 557 | 319 | 0 | 1156 | 308 | 0 | 1025 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay（d），s／veh | 36.5 | 0.0 | 0.0 | 28.0 | 0.0 | 22.9 | 21.9 | 0.0 | 25.3 | 21.9 | 0.0 | 28.1 |
| Incr Delay（d2），s／veh | 381.5 | 0.0 | 0.0 | 5.2 | 0.0 | 0.2 | 30.5 | 0.0 | 7.4 | 1.6 | 0.0 | 8.4 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 42.2 | 0.0 | 0.0 | 9.2 | 0.0 | 2.0 | 6.2 | 0.0 | 18.6 | 1.4 | 0.0 | 15.7 |

Unsig．Movement Delay，s／veh

| LnGrp Delay（d），s／veh | 418.0 | 0.0 | 0.0 | 33.2 | 0.0 | 23.1 | 52.4 | 0.0 | 32.7 | 23.4 | 0.0 | 36.5 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| LnGrp LOS | F |  |  | C |  | C | D |  | C | C |  | D |
| Approach Vol，veh／h |  | 590 |  |  | 545 |  |  | 1127 |  | 779 |  |  |
| Approach Delay，s／veh |  | 418.0 |  |  | 30.9 |  |  | 37.8 |  | 34.7 |  |  |
| Approach LOS |  | F |  |  | C |  |  | D |  |  |  |  |


| Timer - Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$ ，s | 10.3 | 49.7 | 40.0 | 15.0 | 45.1 | 40.0 |
| Change Period（Y＋Rc），s | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Max Green Setting（Gmax），s | 10.0 | 55.0 | 35.0 | 10.0 | 55.0 | 35.0 |
| Max Q Clear Time（g＿c＋1），s | 5.4 | 38.4 | 37.0 | 10.6 | 35.8 | 25.6 |
| Green Ext Time（p＿C），s | 0.2 | 5.4 | 0.0 | 0.0 | 4.3 | 2.3 |

Intersection Summary
HCM 6th Ctrl Delay，s／veh 109.6

HCM 6th LOS
F

|  | 4 |  |  |  |  |  |  | 4 |  |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | $\uparrow$ | 「 | * | $\dagger$ |  | \% | $\hat{F}$ |  |
| Traffic Volume (vph) | 89 | 228 | 225 | 49 | 199 | 115 | 257 | 700 | 38 | 100 | 666 | 69 |
| Future Volume (vph) | 89 | 228 | 225 | 49 | 199 | 115 | 257 | 700 | 38 | 100 | 666 | 69 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 11 | 11 | 11 | 11 | 14 | 14 | 11 | 11 | 11 |
| Grade (\%) |  | -2\% |  |  | 1\% |  |  | -4\% |  |  | -1\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 140 | 256 |  | 0 | 260 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.944 |  |  |  | 0.850 |  | 0.992 |  |  | 0.986 |  |
| Flt Protected |  | 0.992 |  |  | 0.990 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1775 | 0 | 0 | 1795 | 1553 | 1762 | 2031 | 0 | 1754 | 1799 | 0 |
| Flt Permitted |  | 0.751 |  |  | 0.717 |  | 0.078 |  |  | 0.101 |  |  |
| Satd. Flow (perm) | 0 | 1344 | 0 | 0 | 1300 | 1553 | 145 | 2031 | 0 | 186 | 1799 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 32 |  |  |  | 119 |  | 3 |  |  | 6 |  |
| Link Speed (mph) |  | 40 |  |  | 40 |  |  | 40 |  |  | 40 |  |
| Link Distance (ft) |  | 155 |  |  | 698 |  |  | 257 |  |  | 538 |  |
| Travel Time (s) |  | 2.6 |  |  | 11.9 |  |  | 4.4 |  |  | 9.2 |  |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Heavy Vehicles (\%) | 0\% | 1\% | 2\% | 0\% | 1\% | 0\% | 1\% | 1\% | 0\% | 0\% | 1\% | 3\% |
| Adj. Flow (vph) | 92 | 235 | 232 | 51 | 205 | 119 | 265 | 722 | 39 | 103 | 687 | 71 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 559 | 0 | 0 | 256 | 119 | 265 | 761 | 0 | 103 | 758 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  |  |  |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 | 8 | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Minimum Split (s) | 8.0 | 8.0 |  | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 |  | 8.0 | 8.0 |  |
| Total Split (s) | 40.0 | 40.0 |  | 40.0 | 40.0 | 40.0 | 15.0 | 60.0 |  | 15.0 | 60.0 |  |
| Total Split (\%) | 34.8\% | 34.8\% |  | 34.8\% | 34.8\% | 34.8\% | 13.0\% | 52.2\% |  | 13.0\% | 52.2\% |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 5.0 |  |  | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  | Lead | Lag |  | Lead | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes | Yes |  |
| Recall Mode | None | None |  | None | None | None | None | Min |  | None | Min |  |
| Act Effct Green (s) |  | 35.2 |  |  | 35.2 | 35.2 | 61.1 | 51.1 |  | 57.7 | 49.3 |  |
| Actuated g/C Ratio |  | 0.32 |  |  | 0.32 | 0.32 | 0.56 | 0.47 |  | 0.53 | 0.45 |  |
| v/c Ratio |  | 1.23 |  |  | 0.61 | 0.20 | 1.15 | 0.80 |  | 0.47 | 0.93 |  |
| Control Delay (s/veh) |  | 156.2 |  |  | 40.6 | 6.2 | 137.5 | 32.5 |  | 18.2 | 47.5 |  |
| Queue Delay |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay (s/veh) |  | 156.2 |  |  | 40.6 | 6.2 | 137.5 | 32.5 |  | 18.2 | 47.5 |  |
| LOS |  | F |  |  | D | A | F | C |  | B | D |  |
| Approach Delay (s/veh) |  | 156.3 |  |  | 29.7 |  |  | 59.7 |  |  | 44.1 |  |

AMC
Synchro 11 Report
01/16/2024


Splits and Phases: 10: Union Avenue (NYS Route 300) \& South Plank Road (NYS Route 52)


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \$ |  |  | $\stackrel{1}{4}$ | 「 | ${ }^{*}$ | 个 |  | ${ }^{7}$ | F |  |
| Traffic Volume (veh/h) | 89 | 228 | 225 | 49 | 199 | 115 | 257 | 700 | 38 | 100 | 666 | 69 |
| Future Volume (veh/h) | 89 | 228 | 225 | 49 | 199 | 115 | 257 | 700 | 38 | 100 | 666 | 69 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1979 | 1964 | 1949 | 1894 | 1879 | 1894 | 2042 | 2124 | 2140 | 1939 | 1924 | 1894 |
| Adj Flow Rate, veh/h | 92 | 235 | 232 | 51 | 205 | 119 | 265 | 722 | 39 | 103 | 687 | 71 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh, \% | 0 | 1 | 2 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 1 | 3 |
| Cap, veh/h | 92 | 184 | 168 | 97 | 365 | 529 | 296 | 961 | 52 | 294 | 747 | 77 |
| Arrive On Green | 0.33 | 0.33 | 0.33 | 0.33 | 0.33 | 0.33 | 0.09 | 0.48 | 0.48 | 0.05 | 0.44 | 0.44 |
| Sat Flow, veh/h | 159 | 558 | 509 | 171 | 1109 | 1605 | 1945 | 1997 | 108 | 1847 | 1715 | 177 |
| Grp Volume(v), veh/h | 559 | 0 | 0 | 256 | 0 | 119 | 265 | 0 | 761 | 103 | 0 | 758 |
| Grp Sat Flow(s),veh/h/n | 1227 | 0 | 0 | 1280 | 0 | 1605 | 1945 | 0 | 2105 | 1847 | 0 | 1892 |
| Q Serve(g_s), s | 20.7 | 0.0 | 0.0 | 0.0 | 0.0 | 5.7 | 8.1 | 0.0 | 31.2 | 3.2 | 0.0 | 40.1 |
| Cycle Q Clear(g_c), s | 35.0 | 0.0 | 0.0 | 14.3 | 0.0 | 5.7 | 8.1 | 0.0 | 31.2 | 3.2 | 0.0 | 40.1 |
| Prop In Lane | 0.16 |  | 0.42 | 0.20 |  | 1.00 | 1.00 |  | 0.05 | 1.00 |  | 0.09 |
| Lane Grp Cap(c), veh/h | 443 | 0 | 0 | 462 | 0 | 529 | 296 | 0 | 1013 | 294 | 0 | 824 |
| V/C Ratio(X) | 1.26 | 0.00 | 0.00 | 0.55 | 0.00 | 0.23 | 0.90 | 0.00 | 0.75 | 0.35 | 0.00 | 0.92 |
| Avail Cap(c_a), veh/h | 443 | 0 | 0 | 462 | 0 | 529 | 296 | 0 | 1089 | 378 | 0 | 979 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 39.4 | 0.0 | 0.0 | 28.0 | 0.0 | 25.8 | 24.6 | 0.0 | 22.4 | 18.8 | 0.0 | 28.3 |
| Incr Delay (d2), s/veh | 134.4 | 0.0 | 0.0 | 1.4 | 0.0 | 0.2 | 27.7 | 0.0 | 2.8 | 0.7 | 0.0 | 12.1 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ $(50 \%$ ),veh/ln | 28.0 | 0.0 | 0.0 | 5.2 | 0.0 | 2.1 | 5.6 | 0.0 | 15.1 | 1.4 | 0.0 | 19.6 |

Unsig. Movement Delay, s/veh

| LnGrp Delay(d), s/veh | 173.8 | 0.0 | 0.0 | 29.4 | 0.0 | 26.0 | 52.2 | 0.0 | 25.2 | 19.5 | 0.0 | 40.4 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| LnGrp LOS | F |  |  | C |  | C | D |  | C | B |  |  |
| Approach Vol, veh/h |  | 559 |  |  | 375 |  | 1026 |  | D |  |  |  |
| Approach Delay, s/veh | 173.8 |  |  | 28.3 |  | 32.2 |  | 37.9 |  |  |  |  |
| Approach LOS | F |  |  | C |  |  | C |  | D |  |  |  |


| Timer - Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$, s | 10.1 | 56.1 | 40.0 | 15.0 | 51.3 | 40.0 |
| Change Period (Y+Rc), s | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Max Green Setting (Gmax), s | 10.0 | 55.0 | 35.0 | 10.0 | 55.0 | 35.0 |
| Max Q Clear Time (g_c+1), s | 5.2 | 33.2 | 37.0 | 10.1 | 42.1 | 16.3 |
| Green Ext Time (p_c), s | 0.1 | 5.3 | 0.0 | 0.0 | 4.2 | 2.1 |

Intersection Summary
HCM 6th Ctrl Delay, s/veh 61.5
HCM 6th LOS

|  | 4 | $\rightarrow$ |  | 7 |  |  | 4 | $\dagger$ |  | ( | $\frac{1}{\square}$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \& |  |  | $\uparrow$ | F | ${ }^{7}$ | $\uparrow$ |  | ${ }^{1}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 88 | 288 | 212 | 55 | 366 | 122 | 300 | 780 | 48 | 106 | 581 | 87 |
| Future Volume (vph) | 88 | 288 | 212 | 55 | 366 | 122 | 300 | 780 | 48 | 106 | 581 | 87 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 11 | 11 | 11 | 11 | 14 | 14 | 11 | 11 | 11 |
| Grade (\%) |  | -2\% |  |  | 1\% |  |  | -4\% |  |  | -1\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 140 | 256 |  | 0 | 260 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.951 |  |  |  | 0.850 |  | 0.991 |  |  | 0.980 |  |
| Flt Protected |  | 0.993 |  |  | 0.993 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1769 | 0 | 0 | 1794 | 1538 | 1762 | 2027 | 0 | 1702 | 1776 | 0 |
| Flt Permitted |  | 0.502 |  |  | 0.767 |  | 0.129 |  |  | 0.086 |  |  |
| Satd. Flow (perm) | 0 | 894 | 0 | 0 | 1386 | 1538 | 239 | 2027 | 0 | 154 | 1776 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 25 |  |  |  | 86 |  | 4 |  |  | 9 |  |
| Link Speed (mph) |  | 40 |  |  | 40 |  |  | 40 |  |  | 40 |  |
| Link Distance (ft) |  | 155 |  |  | 698 |  |  | 257 |  |  | 538 |  |
| Travel Time (s) |  | 2.6 |  |  | 11.9 |  |  | 4.4 |  |  | 9.2 |  |
| Peak Hour Factor | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 |
| Heavy Vehicles (\%) | 1\% | 4\% | 1\% | 2\% | 1\% | 1\% | 1\% | 1\% | 2\% | 3\% | 2\% | 1\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 594 | 0 | 0 | 426 | 123 | 303 | 836 | 0 | 107 | 675 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 | 8 | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Minimum Split (s) | 8.0 | 8.0 |  | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 |  | 8.0 | 8.0 |  |
| Total Split (s) | 40.0 | 40.0 |  | 40.0 | 40.0 | 40.0 | 15.0 | 60.0 |  | 15.0 | 60.0 |  |
| Total Split (\%) | 34.8\% | 34.8\% |  | 34.8\% | 34.8\% | 34.8\% | 13.0\% | 52.2\% |  | 13.0\% | 52.2\% |  |
| Maximum Green (s) | 35.0 | 35.0 |  | 35.0 | 35.0 | 35.0 | 10.0 | 55.0 |  | 10.0 | 55.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 5.0 |  |  | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  | Lead | Lag |  | Lead | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes | Yes |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | None | Min |  | None | Min |  |
| Act Effct Green (s) |  | 35.3 |  |  | 35.3 | 35.3 | 58.0 | 47.9 |  | 54.9 | 46.3 |  |
| Actuated g/C Ratio |  | 0.33 |  |  | 0.33 | 0.33 | 0.54 | 0.45 |  | 0.51 | 0.43 |  |
| v/c Ratio |  | 1.90 |  |  | 0.93 | 0.21 | 1.10 | 0.91 |  | 0.52 | 0.87 |  |
| Control Delay (s/veh) |  | 443.5 |  |  | 65.6 | 11.8 | 110.1 | 43.4 |  | 23.4 | 39.8 |  |
| Queue Delay |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay (s/veh) |  | 443.5 |  |  | 65.6 | 11.8 | 110.1 | 43.4 |  | 23.4 | 39.8 |  |
| LOS |  | F |  |  | E | B | F | D |  | C | D |  |


| 4 |  |  |  |  |  | , | 4 | \% |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Approach Delay (s/veh) | 443.5 |  |  | 53.6 |  |  | 61.2 |  |  | 37.6 |  |
| Approach LOS | F |  |  | D |  |  | E |  |  | D |  |
| Queue Length 50th ( ft ) | $\sim 654$ |  |  | 298 | 18 | -163 | 518 |  | 31 | 402 |  |
| Queue Length 95th (ft) | \#910 |  |  | \#529 | 65 | \#350 | \#780 |  | 74 | 569 |  |
| Internal Link Dist (ft) | 75 |  |  | 618 |  |  | 177 |  |  | 458 |  |
| Turn Bay Length (ft) |  |  |  |  | 140 | 256 |  |  | 260 |  |  |
| Base Capacity (vph) | 312 |  |  | 457 | 565 | 273 | 1053 |  | 227 | 926 |  |
| Starvation Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 1.90 |  |  | 0.93 | 0.22 | 1.11 | 0.79 |  | 0.47 | 0.73 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 115 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 106.8 |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.90 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay (s/veh): 127.9 |  |  |  | Intersection LOS: F |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 124.4\%Analysis Period (min) 15 |  |  |  | ICU Level of Service H |  |  |  |  |  |  |  |
|  |  |  |  | Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 10: Union Avenue (NYS Route 300) \& South Plank Road (NYS Route 52)


|  | 4 | $\rightarrow$ | 7 | 7 |  |  |  | $\dagger$ | $p$ | V |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \& |  |  | $\uparrow$ | F | ${ }^{*}$ | t |  | \% | $\uparrow$ |  |
| Traffic Volume (vph) | 92 | 232 | 225 | 63 | 190 | 115 | 274 | 702 | 40 | 100 | 671 | 69 |
| Future Volume (vph) | 92 | 232 | 225 | 63 | 190 | 115 | 274 | 702 | 40 | 100 | 671 | 69 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 11 | 11 | 11 | 11 | 14 | 14 | 11 | 11 | 11 |
| Grade (\%) |  | -2\% |  |  | 1\% |  |  | -4\% |  |  | -1\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 140 | 256 |  | 0 | 260 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.945 |  |  |  | 0.850 |  | 0.992 |  |  | 0.986 |  |
| Flt Protected |  | 0.992 |  |  | 0.988 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1777 | 0 | 0 | 1792 | 1553 | 1762 | 2031 | 0 | 1754 | 1799 | 0 |
| Flt Permitted |  | 0.732 |  |  | 0.639 |  | 0.078 |  |  | 0.100 |  |  |
| Satd. Flow (perm) | 0 | 1311 | 0 | 0 | 1159 | 1553 | 145 | 2031 | 0 | 185 | 1799 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 31 |  |  |  | 119 |  | 3 |  |  | 6 |  |
| Link Speed (mph) |  | 40 |  |  | 40 |  |  | 40 |  |  | 40 |  |
| Link Distance (ft) |  | 155 |  |  | 698 |  |  | 257 |  |  | 538 |  |
| Travel Time (s) |  | 2.6 |  |  | 11.9 |  |  | 4.4 |  |  | 9.2 |  |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Heavy Vehicles (\%) | 0\% | 1\% | 2\% | 0\% | 1\% | 0\% | 1\% | 1\% | 0\% | 0\% | 1\% | 3\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 566 | 0 | 0 | 261 | 119 | 282 | 765 | 0 | 103 | 763 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 | 8 | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Minimum Split (s) | 8.0 | 8.0 |  | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 |  | 8.0 | 8.0 |  |
| Total Split (s) | 40.0 | 40.0 |  | 40.0 | 40.0 | 40.0 | 15.0 | 60.0 |  | 15.0 | 60.0 |  |
| Total Split (\%) | 34.8\% | 34.8\% |  | 34.8\% | 34.8\% | 34.8\% | 13.0\% | 52.2\% |  | 13.0\% | 52.2\% |  |
| Maximum Green (s) | 35.0 | 35.0 |  | 35.0 | 35.0 | 35.0 | 10.0 | 55.0 |  | 10.0 | 55.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 5.0 |  |  | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  | Lead | Lag |  | Lead | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes | Yes |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | None | Min |  | None | Min |  |
| Act Effct Green (s) |  | 35.1 |  |  | 35.1 | 35.1 | 61.4 | 51.4 |  | 58.0 | 49.7 |  |
| Actuated g/C Ratio |  | 0.32 |  |  | 0.32 | 0.32 | 0.56 | 0.47 |  | 0.53 | 0.45 |  |
| v/c Ratio |  | 1.28 |  |  | 0.70 | 0.20 | 1.23 | 0.80 |  | 0.47 | 0.93 |  |
| Control Delay (s/veh) |  | 177.3 |  |  | 46.3 | 6.2 | 165.5 | 32.6 |  | 18.2 | 47.9 |  |
| Queue Delay |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay (s/veh) |  | 177.3 |  |  | 46.3 | 6.2 | 165.5 | 32.6 |  | 18.2 | 47.9 |  |
| LOS |  | F |  |  | D | A | F | C |  | B | D |  |


| 4 | $\rightarrow$ |  | 7 |  |  | 4 | $\dagger$ | $p$ | , | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Approach Delay (s/veh) | 177.4 |  |  | 33.8 |  |  | 68.4 |  |  | 44.5 |  |
| Approach LOS | F |  |  | C |  |  | E |  |  | D |  |
| Queue Length 50th ( t ) | $\sim 535$ |  |  | 173 | 0 | $\sim 207$ | 446 |  | 30 | 493 |  |
| Queue Length 95th ( t ) | \#757 |  |  | \#297 | 42 | \#384 | 626 |  | 56 | \#744 |  |
| Internal Link Dist (ft) | 75 |  |  | 618 |  |  | 177 |  |  | 458 |  |
| Turn Bay Length (ft) |  |  |  |  | 140 | 256 |  |  | 260 |  |  |
| Base Capacity (vph) | 440 |  |  | 370 | 577 | 228 | 1029 |  | 244 | 906 |  |
| Starvation Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 1.29 |  |  | 0.71 | 0.21 | 1.24 | 0.74 |  | 0.42 | 0.84 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 115 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 109.9 |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 80 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.29 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay (s/veh): 78.1 |  |  |  | Intersection LOS: E |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 115.9\% |  |  |  | ICU Level of Service H |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 10: Union Avenue (NYS Route 300) \& South Plank Road (NYS Route 52)


|  | 4 | $\rightarrow$ | 7 | 7 |  |  |  | $\dagger$ | $p$ | ( | $\frac{1}{\square}$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | $\uparrow$ | 7 | \% | $\uparrow$ |  | \% | $\uparrow$ |  |
| Traffic Volume (vph) | 88 | 288 | 212 | 55 | 366 | 122 | 300 | 780 | 48 | 106 | 581 | 87 |
| Future Volume (vph) | 88 | 288 | 212 | 55 | 366 | 122 | 300 | 780 | 48 | 106 | 581 | 87 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 11 | 11 | 11 | 11 | 14 | 14 | 11 | 11 | 11 |
| Grade (\%) |  | -2\% |  |  | 1\% |  |  | -4\% |  |  | -1\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 140 | 256 |  | 0 | 260 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.951 |  |  |  | 0.850 |  | 0.991 |  |  | 0.980 |  |
| Flt Protected |  | 0.993 |  |  | 0.993 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1769 | 0 | 0 | 1794 | 1538 | 1762 | 2027 | 0 | 1702 | 1776 | 0 |
| Flt Permitted |  | 0.510 |  |  | 0.770 |  | 0.115 |  |  | 0.087 |  |  |
| Satd. Flow (perm) | 0 | 908 | 0 | 0 | 1391 | 1538 | 213 | 2027 | 0 | 156 | 1776 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 26 |  |  |  | 87 |  | 4 |  |  | 9 |  |
| Link Speed (mph) |  | 40 |  |  | 40 |  |  | 40 |  |  | 40 |  |
| Link Distance (ft) |  | 155 |  |  | 698 |  |  | 257 |  |  | 538 |  |
| Travel Time (s) |  | 2.6 |  |  | 11.9 |  |  | 4.4 |  |  | 9.2 |  |
| Peak Hour Factor | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 |
| Heavy Vehicles (\%) | 1\% | 4\% | 1\% | 2\% | 1\% | 1\% | 1\% | 1\% | 2\% | 3\% | 2\% | 1\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 594 | 0 | 0 | 426 | 123 | 303 | 836 | 0 | 107 | 675 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 | 8 | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Minimum Split (s) | 8.0 | 8.0 |  | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 |  | 8.0 | 8.0 |  |
| Total Split (s) | 41.0 | 41.0 |  | 41.0 | 41.0 | 41.0 | 16.0 | 58.0 |  | 16.0 | 58.0 |  |
| Total Split (\%) | 35.7\% | 35.7\% |  | 35.7\% | 35.7\% | 35.7\% | 13.9\% | 50.4\% |  | 13.9\% | 50.4\% |  |
| Maximum Green (s) | 36.0 | 36.0 |  | 36.0 | 36.0 | 36.0 | 11.0 | 53.0 |  | 11.0 | 53.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 5.0 |  |  | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  | Lead | Lag |  | Lead | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes | Yes |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | None | Min |  | None | Min |  |
| Act Effct Green (s) |  | 36.2 |  |  | 36.2 | 36.2 | 59.2 | 48.1 |  | 54.8 | 45.9 |  |
| Actuated g/C Ratio |  | 0.33 |  |  | 0.33 | 0.33 | 0.55 | 0.44 |  | 0.51 | 0.42 |  |
| v/c Ratio |  | 1.85 |  |  | 0.91 | 0.21 | 1.10 | 0.92 |  | 0.52 | 0.89 |  |
| Control Delay (s/veh) |  | 419.4 |  |  | 62.5 | 11.4 | 110.6 | 45.4 |  | 23.3 | 43.5 |  |
| Queue Delay |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay (s/veh) |  | 419.4 |  |  | 62.5 | 11.4 | 110.6 | 45.4 |  | 23.3 | 43.5 |  |
| LOS |  | F |  |  | E | B | F | D |  | C | D |  |



Splits and Phases: 10: Union Avenue (NYS Route 300) \& South Plank Road (NYS Route 52)


|  | 4 | $\rightarrow$ | 7 | 7 |  |  |  | $\dagger$ | $p$ | ( |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \& |  |  | $\uparrow$ | F | ${ }^{*}$ | F |  | \% | $\uparrow$ |  |
| Traffic Volume (vph) | 92 | 232 | 225 | 63 | 190 | 115 | 274 | 702 | 40 | 100 | 671 | 69 |
| Future Volume (vph) | 92 | 232 | 225 | 63 | 190 | 115 | 274 | 702 | 40 | 100 | 671 | 69 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 11 | 11 | 11 | 11 | 14 | 14 | 11 | 11 | 11 |
| Grade (\%) |  | -2\% |  |  | 1\% |  |  | -4\% |  |  | -1\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 140 | 256 |  | 0 | 260 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.945 |  |  |  | 0.850 |  | 0.992 |  |  | 0.986 |  |
| Flt Protected |  | 0.992 |  |  | 0.988 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1777 | 0 | 0 | 1792 | 1553 | 1762 | 2031 | 0 | 1754 | 1799 | 0 |
| Flt Permitted |  | 0.740 |  |  | 0.647 |  | 0.077 |  |  | 0.092 |  |  |
| Satd. Flow (perm) | 0 | 1325 | 0 | 0 | 1174 | 1553 | 143 | 2031 | 0 | 170 | 1799 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 32 |  |  |  | 119 |  | 3 |  |  | 6 |  |
| Link Speed (mph) |  | 40 |  |  | 40 |  |  | 40 |  |  | 40 |  |
| Link Distance (ft) |  | 155 |  |  | 698 |  |  | 257 |  |  | 538 |  |
| Travel Time (s) |  | 2.6 |  |  | 11.9 |  |  | 4.4 |  |  | 9.2 |  |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Heavy Vehicles (\%) | 0\% | 1\% | 2\% | 0\% | 1\% | 0\% | 1\% | 1\% | 0\% | 0\% | 1\% | 3\% |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 566 | 0 | 0 | 261 | 119 | 282 | 765 | 0 | 103 | 763 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 | 8 | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Minimum Split (s) | 8.0 | 8.0 |  | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 |  | 8.0 | 8.0 |  |
| Total Split (s) | 42.0 | 42.0 |  | 42.0 | 42.0 | 42.0 | 16.0 | 57.0 |  | 16.0 | 57.0 |  |
| Total Split (\%) | 36.5\% | 36.5\% |  | 36.5\% | 36.5\% | 36.5\% | 13.9\% | 49.6\% |  | 13.9\% | 49.6\% |  |
| Maximum Green (s) | 37.0 | 37.0 |  | 37.0 | 37.0 | 37.0 | 11.0 | 52.0 |  | 11.0 | 52.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 5.0 |  |  | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  | Lead | Lag |  | Lead | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes | Yes |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | None | Min |  | None | Min |  |
| Act Effct Green (s) |  | 37.1 |  |  | 37.1 | 37.1 | 63.2 | 52.2 |  | 58.6 | 49.9 |  |
| Actuated g/C Ratio |  | 0.33 |  |  | 0.33 | 0.33 | 0.56 | 0.46 |  | 0.52 | 0.44 |  |
| v/c Ratio |  | 1.24 |  |  | 0.67 | 0.20 | 1.18 | 0.81 |  | 0.49 | 0.95 |  |
| Control Delay (s/veh) |  | 158.6 |  |  | 43.9 | 5.9 | 147.3 | 34.7 |  | 20.8 | 53.9 |  |
| Queue Delay |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay (s/veh) |  | 158.6 |  |  | 43.9 | 5.9 | 147.3 | 34.7 |  | 20.8 | 53.9 |  |
| LOS |  | F |  |  | D | A | F | C |  | C | D |  |


| $\Rightarrow$ | $\rightarrow$ |  |  |  |  | 4 | $\dagger$ | $p$ |  | 1 | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Approach Delay (s/veh) | 158.6 |  |  | 32.0 |  |  | 65.1 |  |  | 50.0 |  |
| Approach LOS | F |  |  | C |  |  | E |  |  | D |  |
| Queue Length 50th (ft) | $\sim 513$ |  |  | 168 | 0 | $\sim 200$ | 463 |  | 31 | 520 |  |
| Queue Length 95th (ft) | \#735 |  |  | 269 | 41 | \#379 | 661 |  | 65 | \#782 |  |
| Internal Link Dist (ft) | 75 |  |  | 618 |  |  | 177 |  |  | 458 |  |
| Turn Bay Length (ft) |  |  |  |  | 140 | 256 |  |  | 260 |  |  |
| Base Capacity (vph) | 456 |  |  | 384 | 589 | 238 | 961 |  | 245 | 832 |  |
| Starvation Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 1.24 |  |  | 0.68 | 0.20 | 1.18 | 0.80 |  | 0.42 | 0.92 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 115 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 113 |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 80 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.24 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay (s/veh): 74.6 Intersection LOS: E |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 115.9\% ICU Level of Service H |  |  |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 10: Union Avenue (NYS Route 300) \& South Plank Road (NYS Route 52)





| Major/Minor | Minor2 |  | Major1 | Major2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 2112 | 1005 | 1020 | 0 | - | 0 |  |
| Stage 1 | 1005 | - | - | - | - | - |  |
| Stage 2 | 1107 | - | - | - | - | - |  |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - |  |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |  |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - |  |
| Pot Cap-1 Maneuver | 56 | 293 | 680 | - | - | - |  |
| Stage 1 | 354 | - | - | - | - | - |  |
| Stage 2 | 316 | - | - | - | - | - |  |
| Platoon blocked, \% |  |  |  | - | - | - |  |
| Mov Cap-1 Maneuver | 53 | 293 | 680 | - | - | - |  |
| Mov Cap-2 Maneuver | 173 | - | - | - | - | - |  |
| Stage 1 | 338 | - | - | - | - | - |  |
| Stage 2 | 316 | - | - | - | - | - |  |


| Approach | EB | NB |
| :--- | ---: | ---: |
| HCM Control Delay, s/v 28.8 | 0.3 | 0 |

HCMLOS D

| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |
| :--- | ---: | ---: | ---: | :---: |
| Capacity (veh/h) | 680 | -211 | - | - |
| HCM Lane V/C Ratio | 0.045 | -0.287 | - | - |
| HCM Control Delay (s/veh) | 10.5 | -28.8 | - | - |
| HCM Lane LOS | $B$ | - | $D$ | - |
| HCM 95th \%tile Q (veh) | 0.1 | - | 1.1 | - |
| (ven |  |  |  |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Major1 | Major2 | Minor1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 - | - |  | 616 |
| Stage 1 | - | - - | - | - | - |
| Stage 2 | - | - - | - | - |  |
| Critical Hdwy | - | - - | - | - | 6.22 |
| Critical Hdwy Stg 1 | - | - - | - | - |  |
| Critical Hdwy Stg 2 | - | - - | - | - |  |
| Follow-up Hdwy | - | - - | - | - | 3.318 |
| Pot Cap-1 Maneuver | - | - 0 | - | 0 | 491 |
| Stage 1 | - | - 0 | - | 0 | - |
| Stage 2 | - | - 0 | - | 0 |  |
| Platoon blocked, \% | - | - | - |  |  |
| Mov Cap-1 Maneuver | - | - - | - | - | 491 |
| Mov Cap-2 Maneuver | - | - - | - | - | - |
| Stage 1 | - | - - | - | - |  |
| Stage 2 | - | - - | - | - |  |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s/v | 0 | 0 | 12.5 |

HCMLOS B

| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBT |
| :--- | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 491 | - | - | - |
| HCM Lane V/C Ratio | 0.017 | - | - | - |
| HCM Control Delay (s/veh) | 12.5 | - | - | - |
| HCM Lane LOS | B | - | - | - |
| HCM 95th \%tile Q (veh) | 0.1 | - | - | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | F |  |  | A |  | $\mathbf{F}$ |
| Traffic Vol, veh/h | 537 | 14 | 0 | 533 | 0 | 12 |
| Future Vol, veh/h | 537 | 14 | 0 | 533 | 0 | 12 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | -1 | - | - | 3 | 0 | - |
| Peak Hour Factor | 98 | 98 | 98 | 98 | 98 | 98 |
| Heavy Vehicles, $\%$ | 1 | 2 | 2 | 1 | 2 | 2 |
| Mvmt Flow | 548 | 14 | 0 | 544 | 0 | 12 |


| Major/Minor | Major1 | Major2 |  | Minor1 |  |
| :--- | ---: | :--- | :--- | :--- | :--- |
| Conflicting Flow All | 0 | 0 | - | - | - |
| $\quad$ Stage 1 | - | - | - | - | - |
| $\quad$ Stage 2 | - | - | - | - | - |


|  | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| Approach | 0 | 11.9 |  |
| HCM Control Delay, s/v | 0 | 0 | $B$ |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBT |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 531 | - | - | - |
| HCM Lane V/C Ratio | 0.023 | - | - | - |
| HCM Control Delay (s/veh) | 11.9 | - | - | - |
| HCM Lane LOS | $B$ | - | - | - |
| HCM 95th \%tile Q (veh) | 0.1 | - | - | - |

